

# X-parameter applications for characterizing and modeling power amplifiers for envelope tracking applications

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more details in session TU3F-1 Tues 13:50-14:10 ref [21]

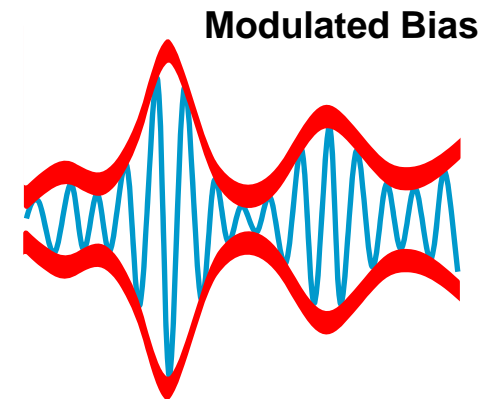
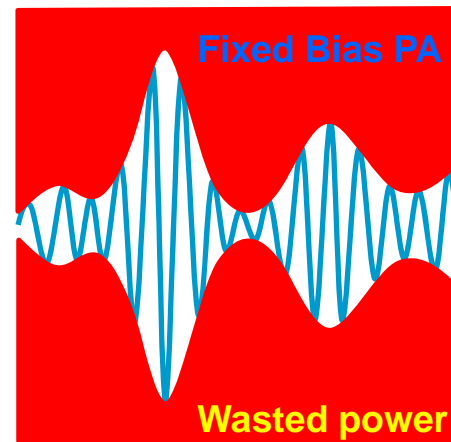
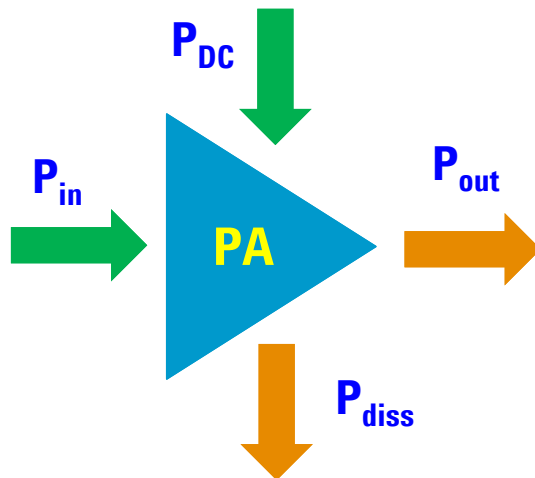


# Outline

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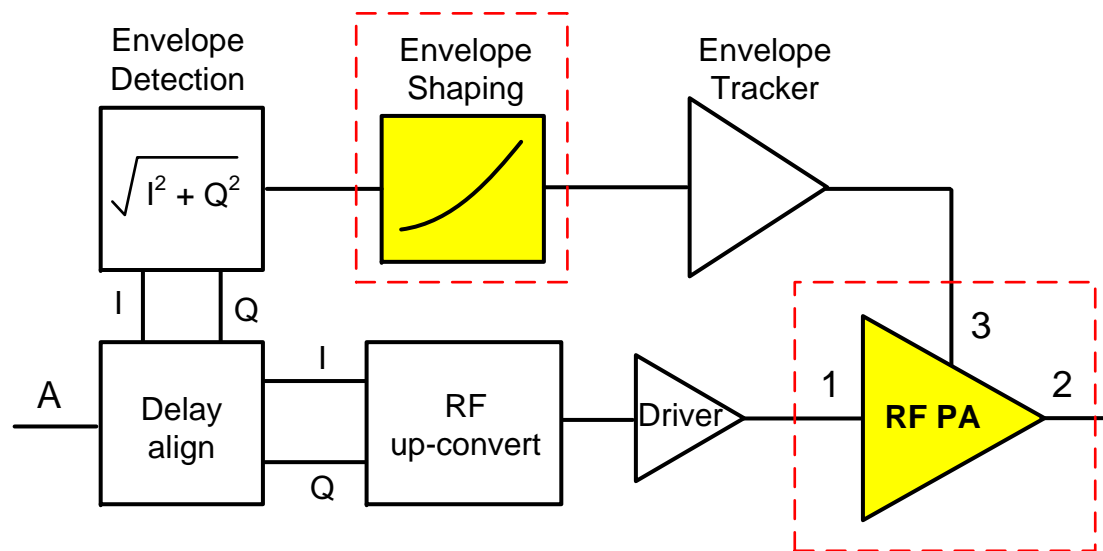
- Introduction to ET
- Introduction to X-parameters
- X-parameter models for dynamic signals: quasi-static approximation
- Simulation-based X-parameter models for ET applications
- Measurement-based GaN PA X-parameter model
- Future work
- Conclusions

# Envelope tracking



$$PAE = \frac{P_{out} - P_{in}}{P_{DC}} = (G - 1) \frac{P_{in}}{P_{DC}} = (G - 1) \frac{V_{in} I_{in}}{V_{DC} I_{DC}}$$

# Envelope tracking

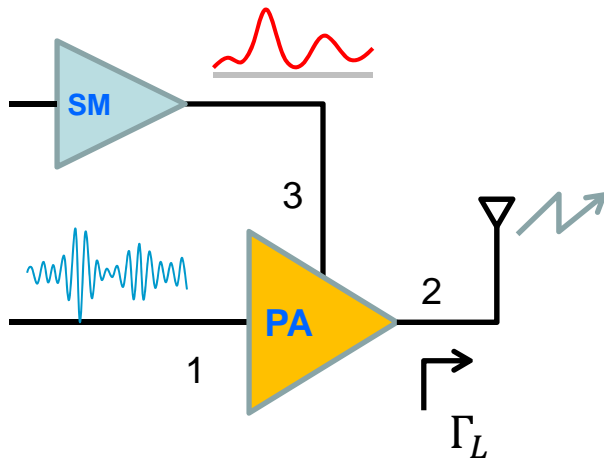


Shaping table depends on the properties of the RF PA,  
*viewed as a three-terminal component.*

X-parameters provides a procedural approach to characterize & model the RF PA for shaping table design, including bias and load effects.

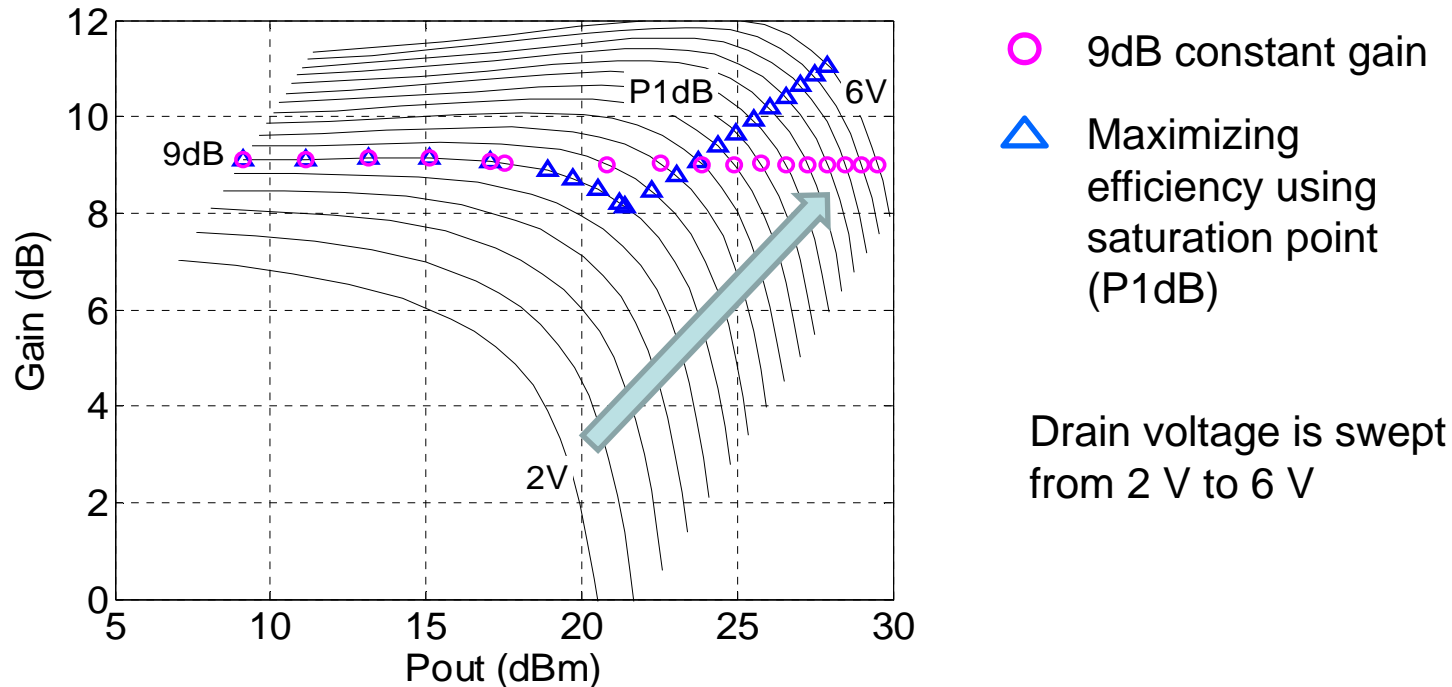
# Envelope tracking

- Design considerations with ET
  - High PAR input signals
  - Varying supply voltage
  - Varying load
- XP model, which is a frequency domain black box behavioral model, is studied
- Design and characterization assumption:
  - SM is ideal
  - Interconnection impedance is minimum
  - PA is quasi-static to the supply voltage variation
  - Load is approximately matched (but more on this later)



# Envelope tracking

Practical approach is designing the shaping using static characterization at multiple supply voltages under quasi-static assumption of the PA

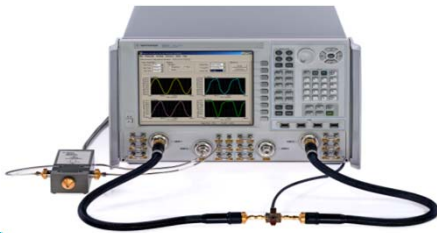


# X-parameters

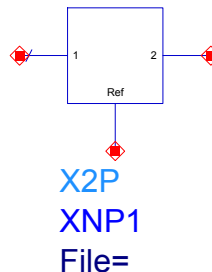
X-parameters are the scientifically correct extension of S-parameters to large-signal conditions.

- Measurement and simulation based, identifiable from a simple set of automated NVNA measurements or directly from ADS circuit-level designs
- Vector nonlinearities (Magnitude *and* phase of distortion)
- Intrinsic DUT properties (calibrates out source impurities & multi-freq. mismatch)
- Cascadable (correct behavior in mismatched environment)
- Extremely accurate for high-frequency, distributed nonlinear devices
- Includes bias dependence

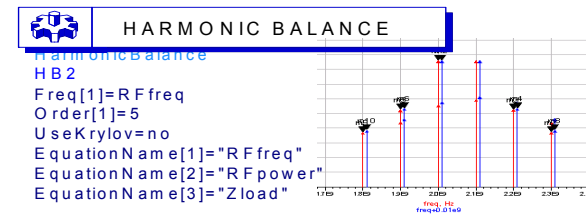
Measure X-parameters  
-or-  
Generate X-parameters from  
circuit-level designs



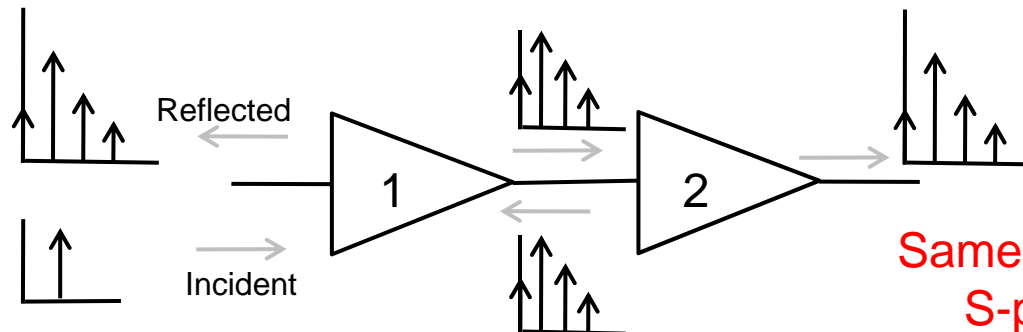
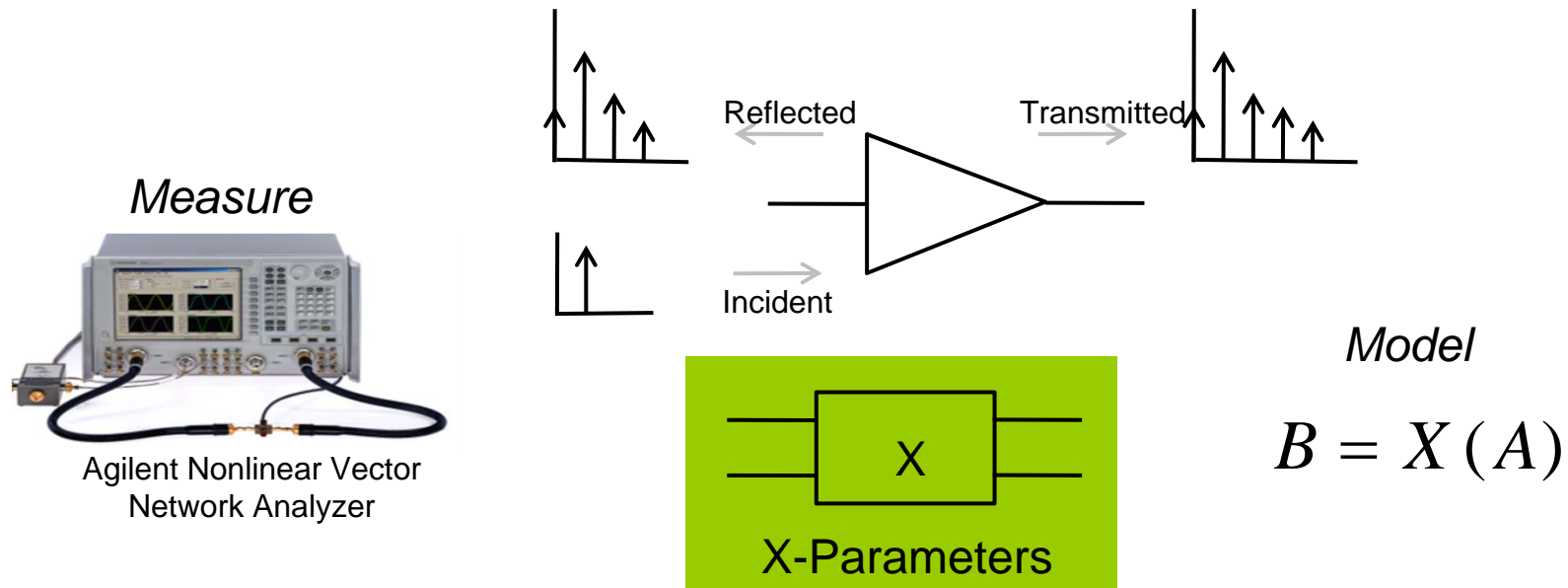
X-parameter Component :  
Simulate using X-  
parameters



ADS, SystemVue & Genesys:  
Design using X-parameters



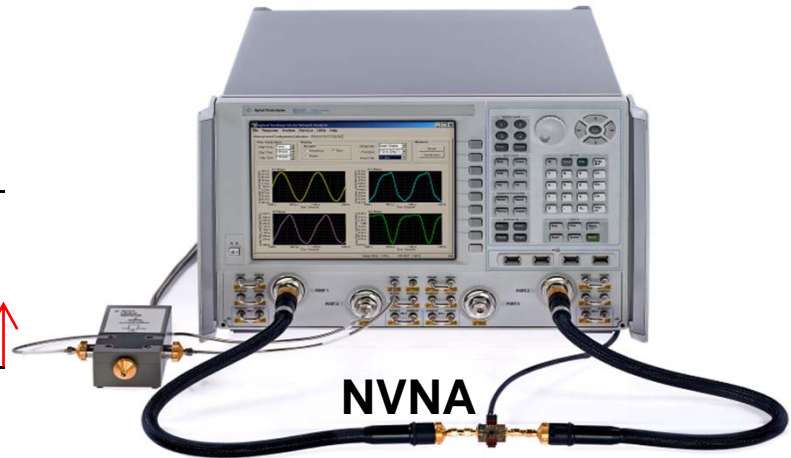
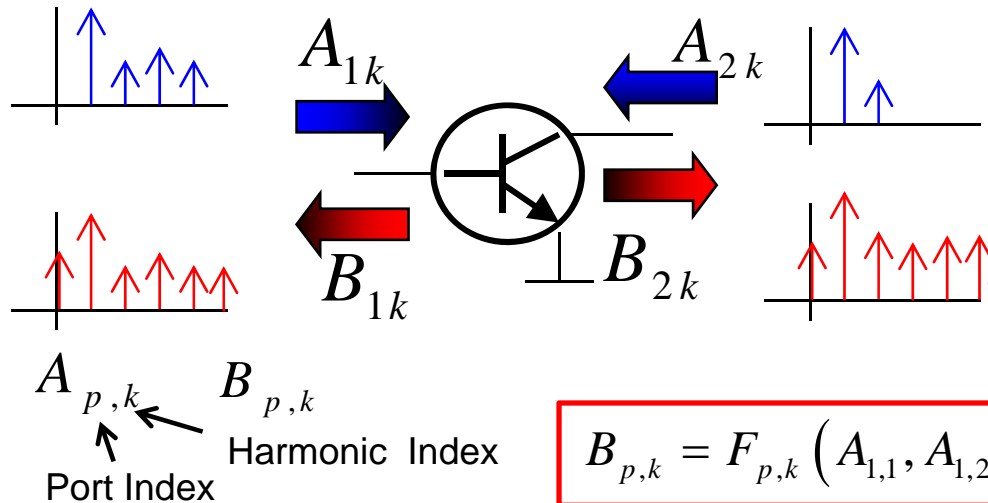
# X-parameter use model



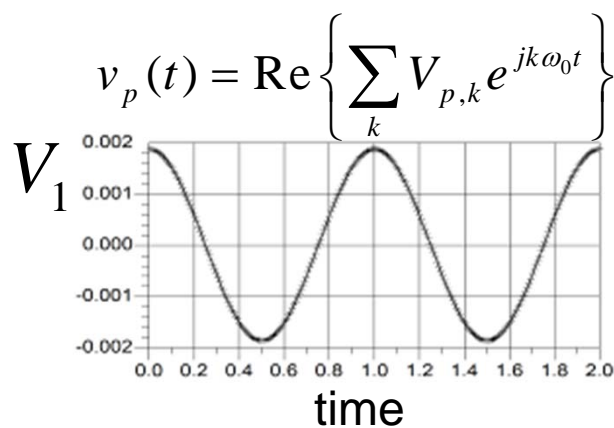
Same use model as  
S-parameters  
*but much more powerful*



# Complex Spectra and Nonlinear Maps

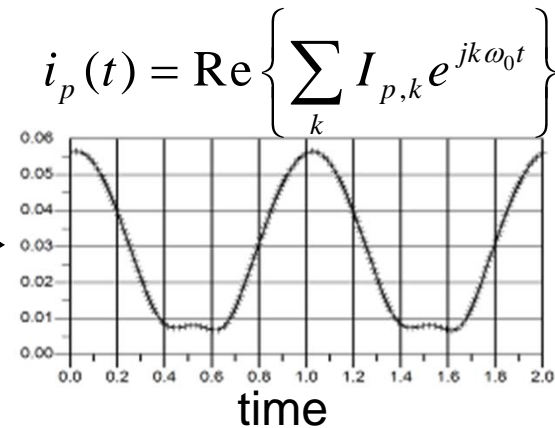


$$B_{p,k} = F_{p,k} (A_{1,1}, A_{1,2}, A_{1,3}, \dots, A_{2,1}, A_{2,2}, A_{2,3}, \dots)$$



$$V_{p,k} = \sqrt{2Z_0} \cdot (A_{p,k} + B_{p,k})$$

$$I_{p,k} = \sqrt{\frac{2}{Z_0}} \cdot (A_{p,k} - B_{p,k}) I_2$$





# Time-invariance and spectral linearization

X-parameters allow us to **simplify** the general B(A) relations:  
Trade efficiency, practicality, for generality & accuracy  
**Powerful, correct, and practical; Native Freq. Domain Model**

DC dependence automatically included. NVNA controls DC supplies and synchronizes measurements with applied RF signal

$$B_i = S_{i1}(DC)A_1 + S_{i2}(DC)A_2$$

The simplest X-parameters are just linear S-parameters

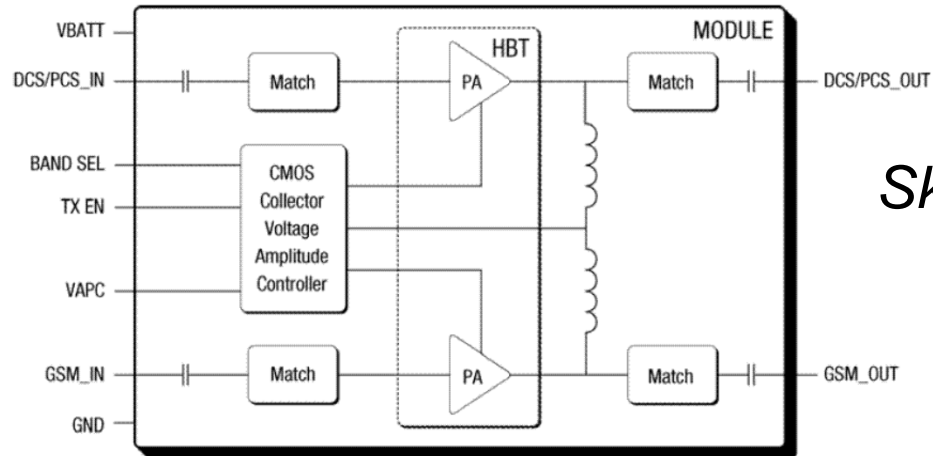
$$B_{e,f} = X_{ef}^{(F)}(DC, |A_{11}|)P^f + \sum_{g,h} X_{ef,gh}^{(S)}(DC, |A_{11}|)P^{f-h} \cdot A_{gh} + \sum_{g,h} X_{ef,gh}^{(T)}(DC, |A_{11}|)P^{f+h} \cdot A_{gh}^*$$

matched response

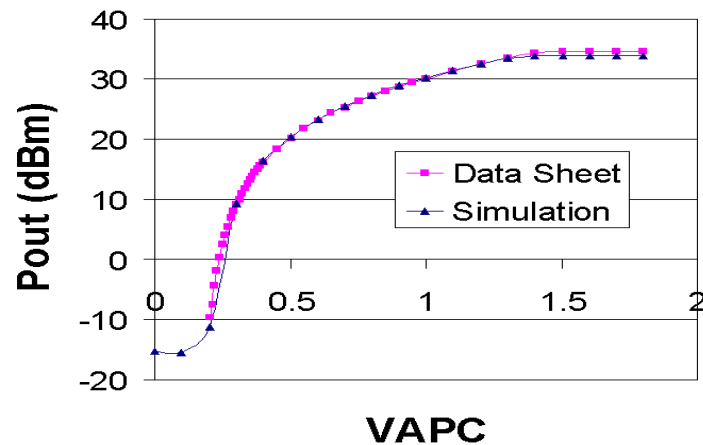
*load & harmonic mismatch*

*new mismatch terms*

# X-parameters of GSM PA

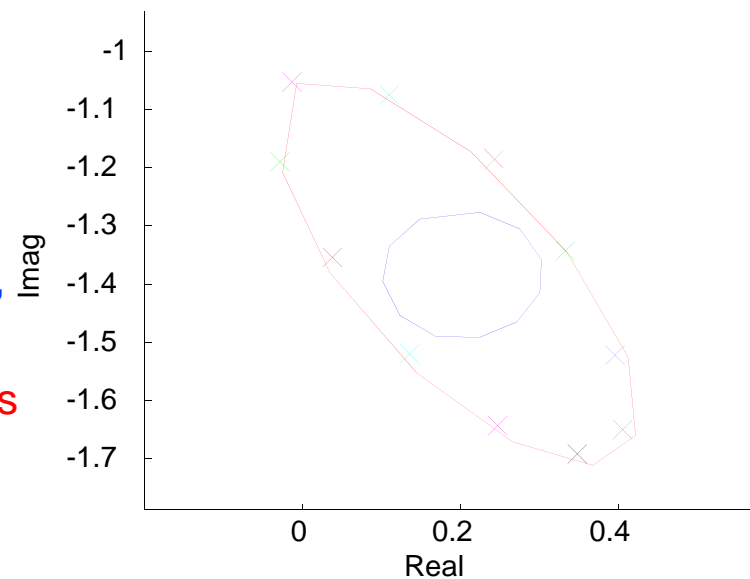


Skyworks amp



measured  
— “Hot  $S_{22}$ ”  
— X-params

Mismatch versus phase at GSM\_OUT

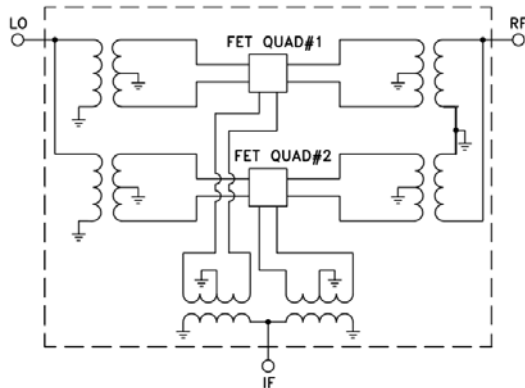


Horn et al., EuMC 2009

*“X-parameters provide a nonlinear electronic interactive datasheet”*

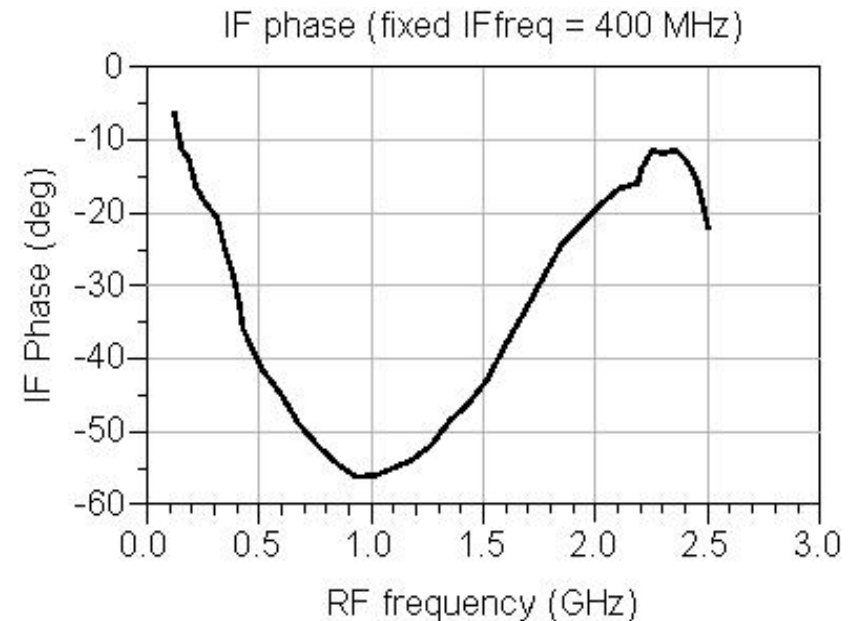
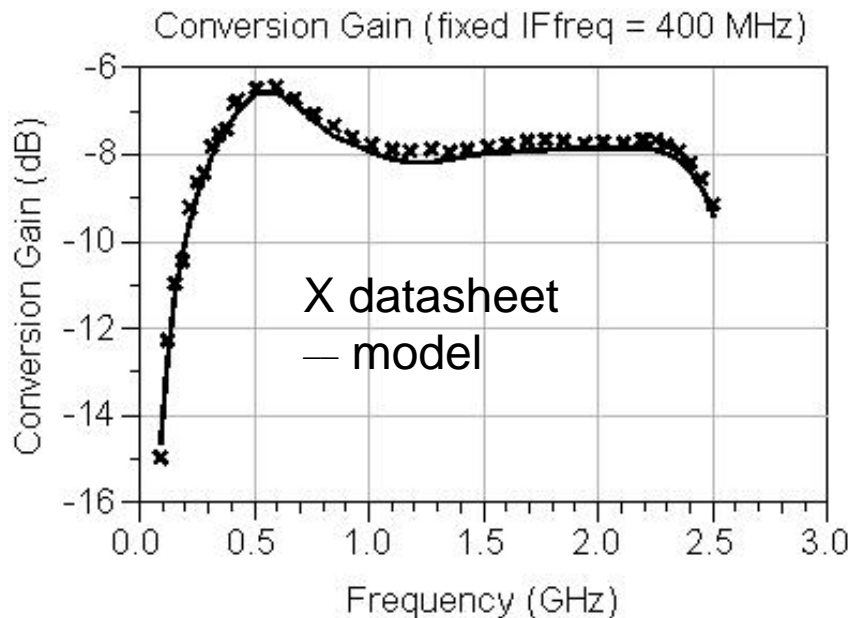
# X-parameters of mixers: 3 rf ports

electrical schematic

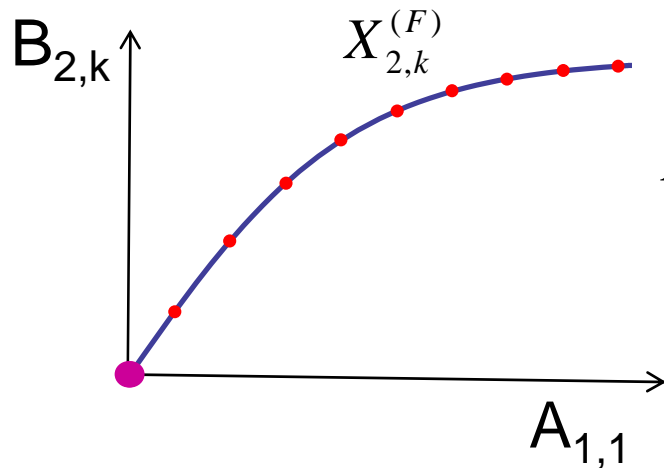


Mini-Circuits  
LAVI-22VH+ (TB-433)  
Double-balanced Mixer  
**3-ports**

New measurement: IF Phase!



# Simulation of dynamic signals



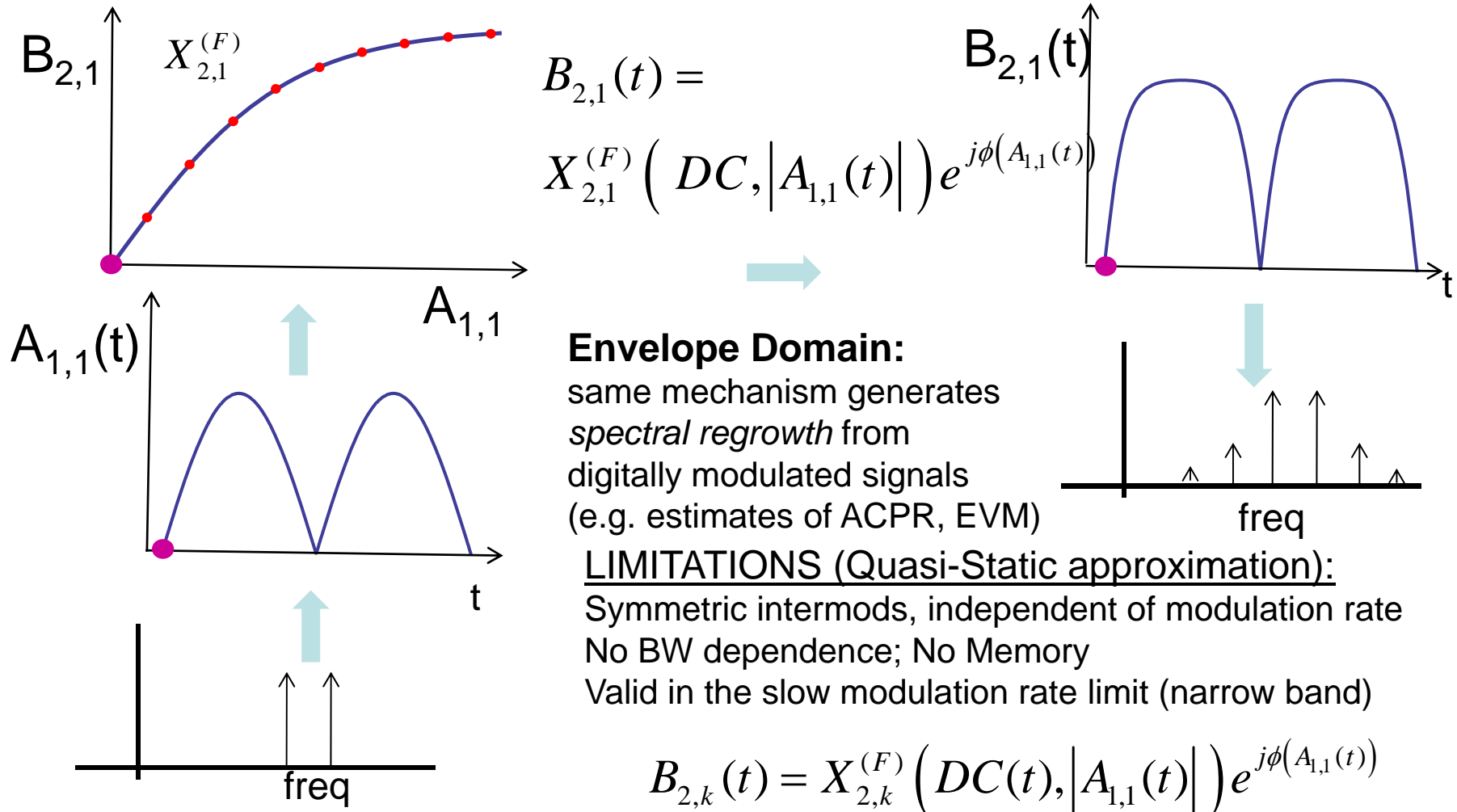
$$B_{2,k} = X_{2,k}^{(F)} \left( DC, |A_{1,1}| \right) e^{j\phi(A_{1,1})}$$

Now assume the signal is modulated in time:  $A_{2,1} \rightarrow A_{2,1}(t)$

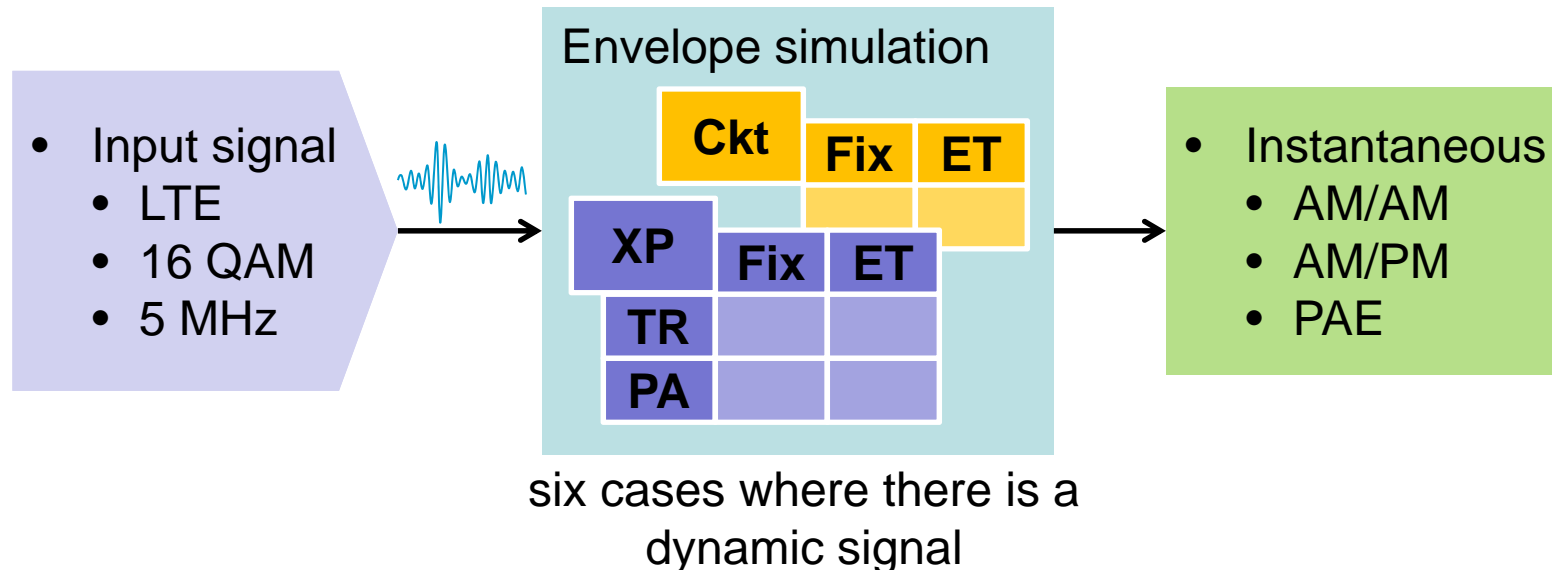
**Quasi-static approximation:** evaluate static X-parameter function at each time instant

$$B_{2,k}(t) = X_{2,k}^{(F)} \left( DC, |A_{1,1}(t)| \right) e^{j\phi(A_{1,1}(t))}$$

# Simulating Dynamic signals (2)



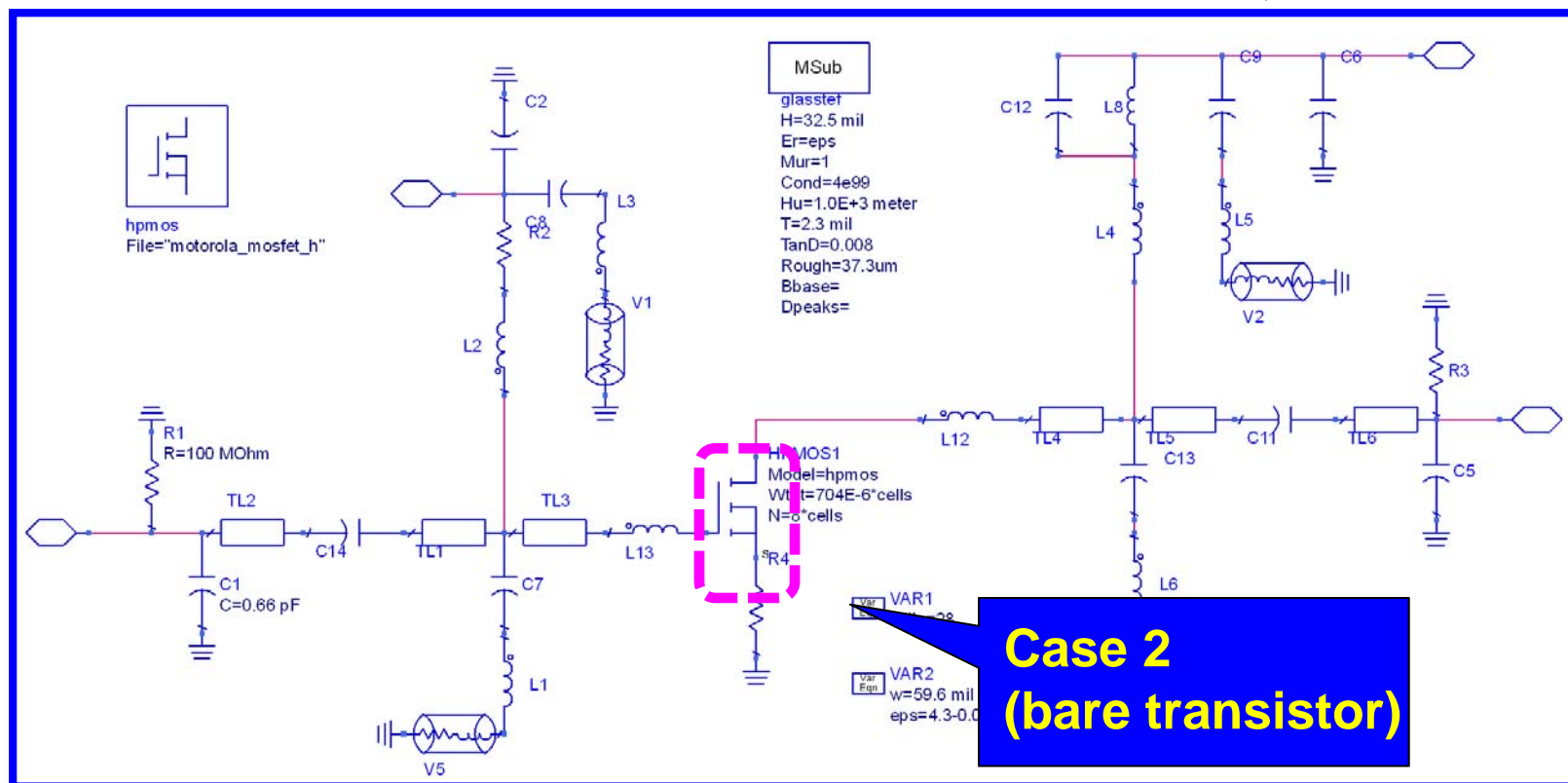
# Simulation-based approach



- XP models are extracted in two cases to show the sources of dynamic response contribution
  - entire circuit
  - bare transistor
- Fixed bias performance is compared to ET operation for the reference circuit model and the two X-parameter models

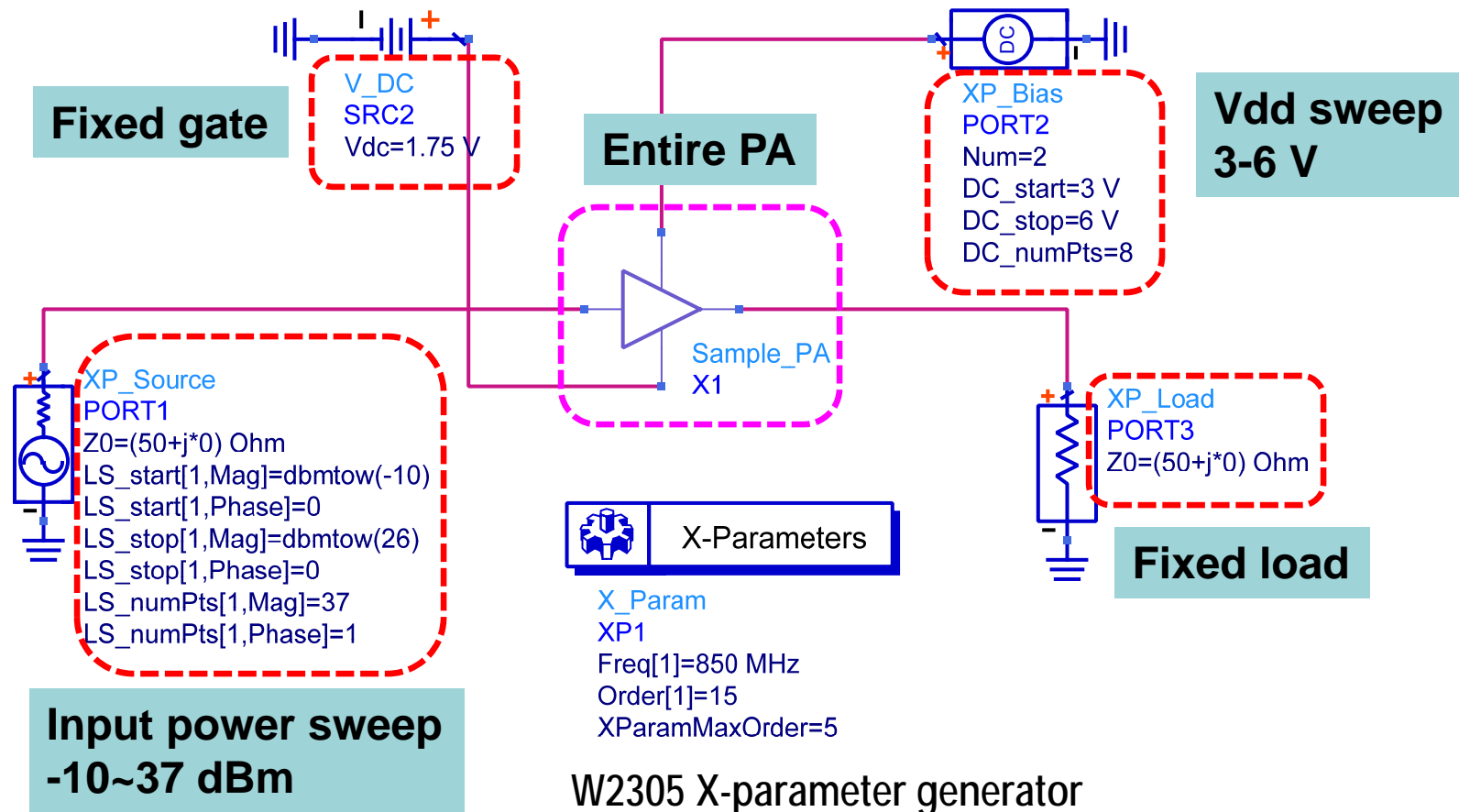
# Simulation-based extraction

**Case 1  
(whole PA)**

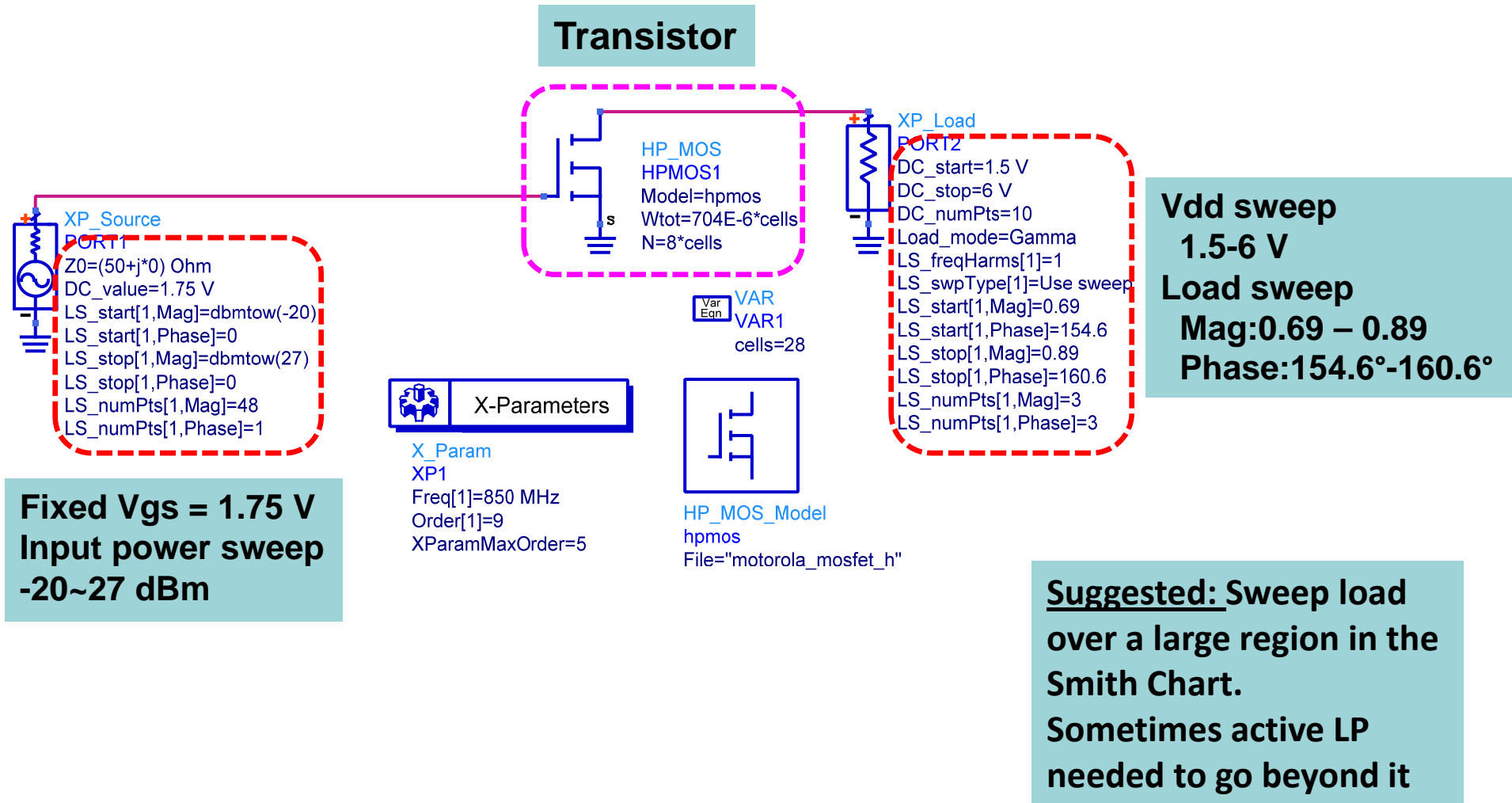


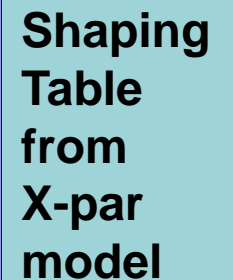


# Generating the X-parameters (1)



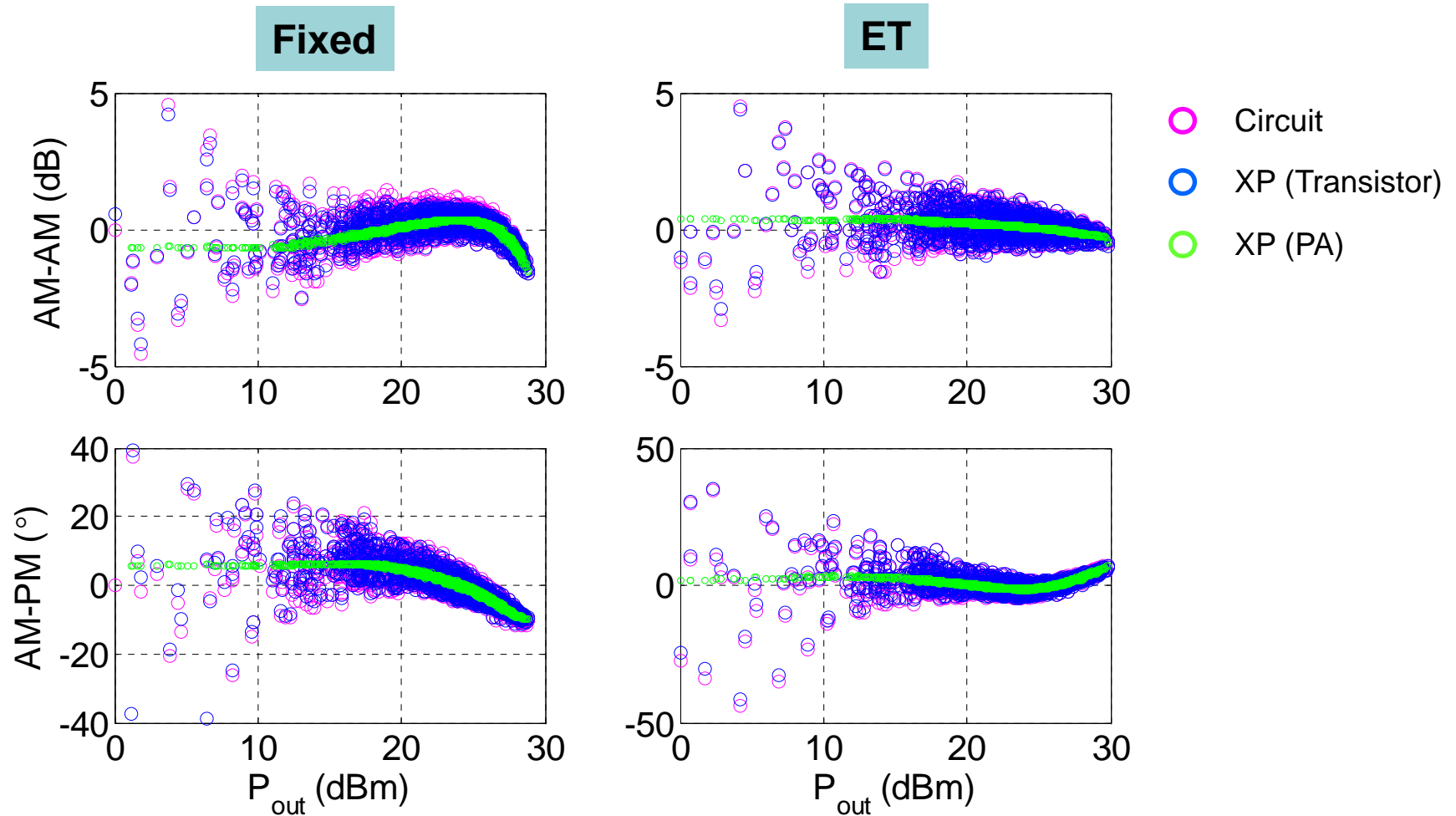
# Generating the X-parameters (2)



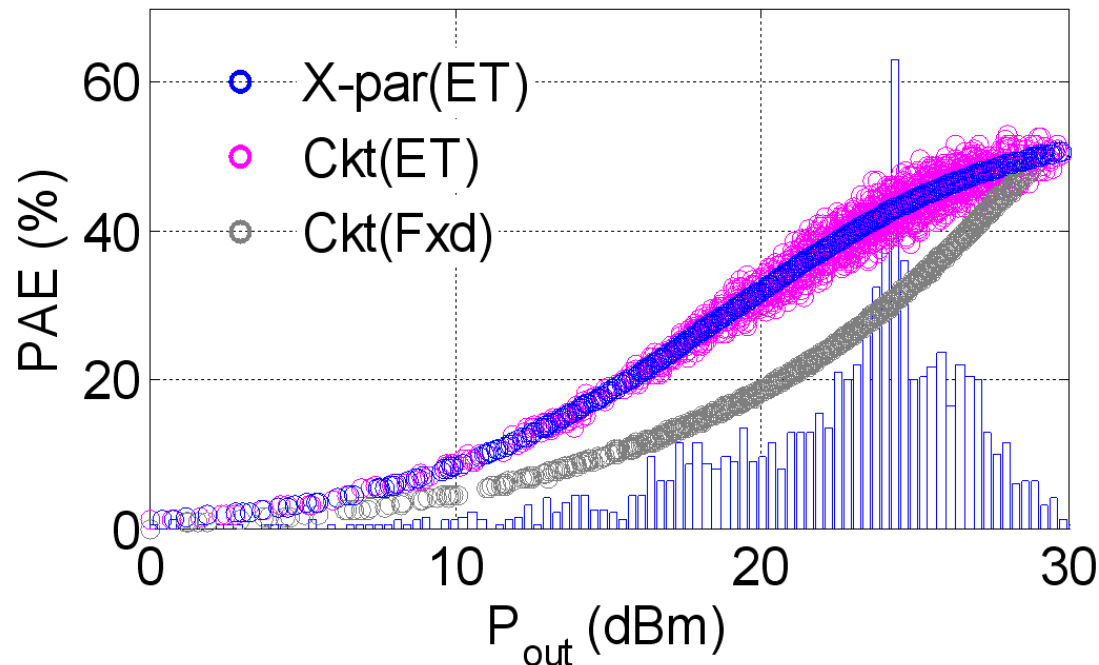


ADS ET examples can be downloaded from [1]:  
<http://edocs.soco.agilent.com/display/eesofkcds/Applying+envelope+tracking+to+Improve+Efficiency>

# Simulation-based validation



# Simulation-based validation

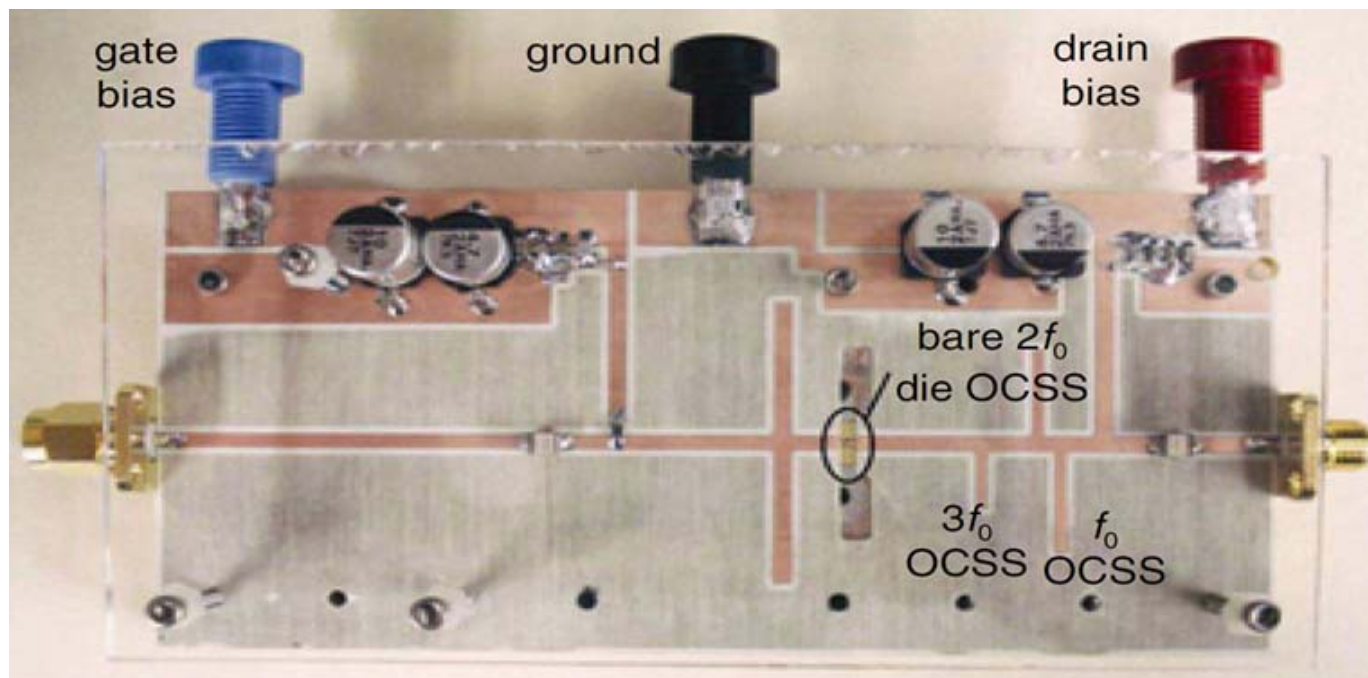


PAE <sub>avg</sub> (%)	
XP(ET)	43.3
Ckt(ET)	42.4
Ckt(Fix)	31.7

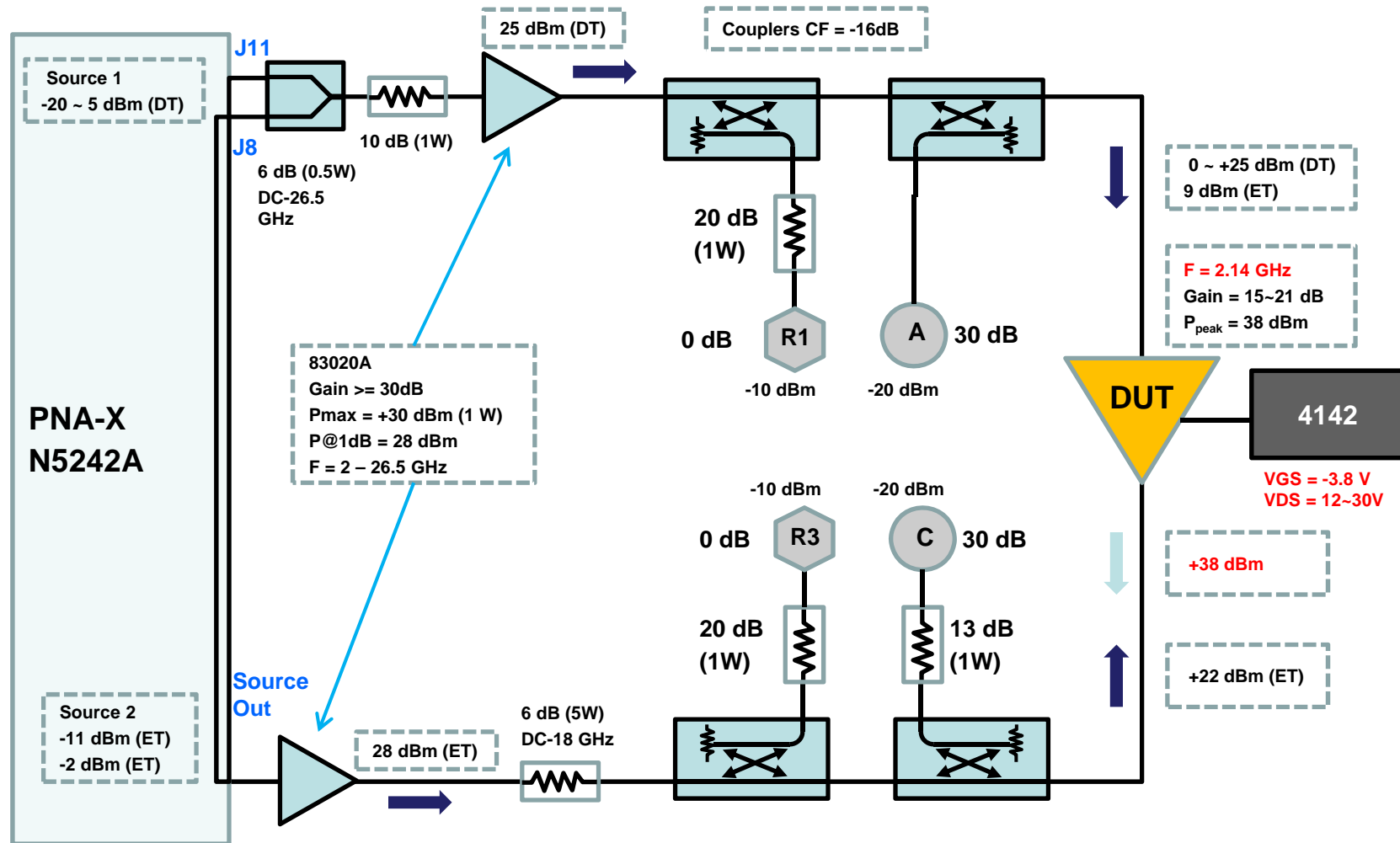
- Instantaneous PAE was calculated using LTE signals and drawn over the histogram of the signals.
- Both XP and circuit model predict PAE improvement over fixed bias as expected.
- It is interesting to notice that, under ET, the instantaneous PAE predicted by the circuit model shows wider spreading than fixed bias.

# Measurement-based X-parameters

- GaN HEMT 8 W Class-F<sup>-1</sup> (Triquint TGF2023-02)
- Drain voltage sweep : 12 ~ 30 V
- Load-pull performed with *VTD SWAP-X402* (now Agilent)



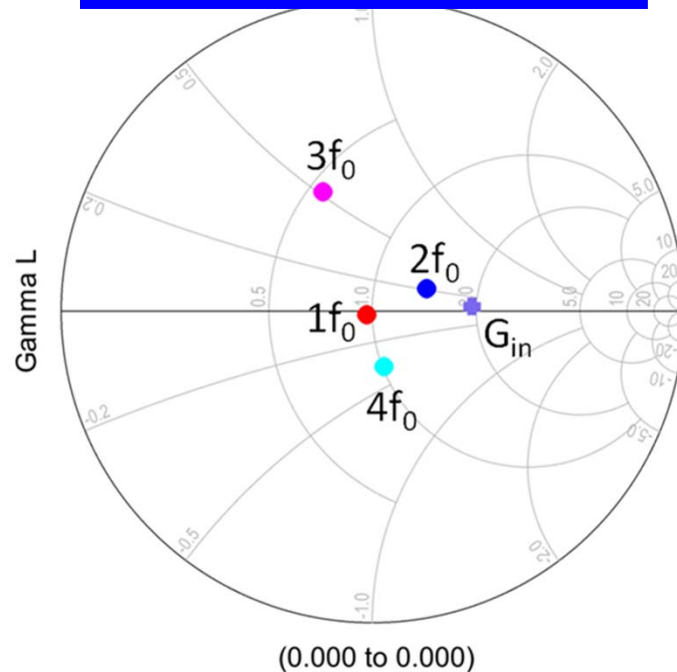
# X-par extraction for 8 W GaN PA



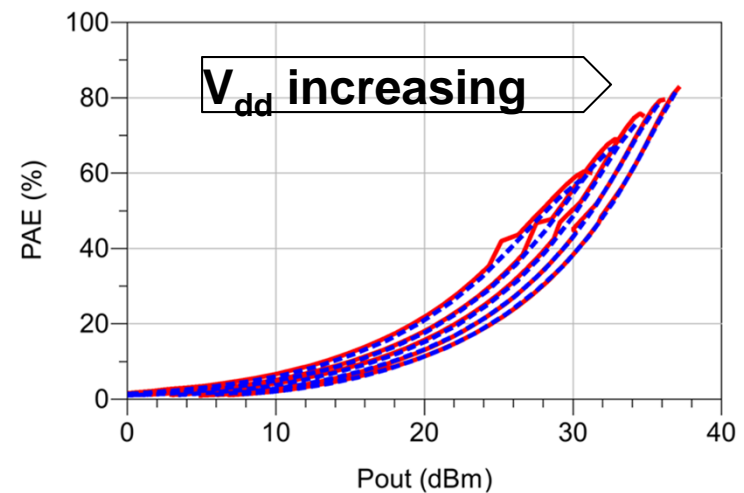
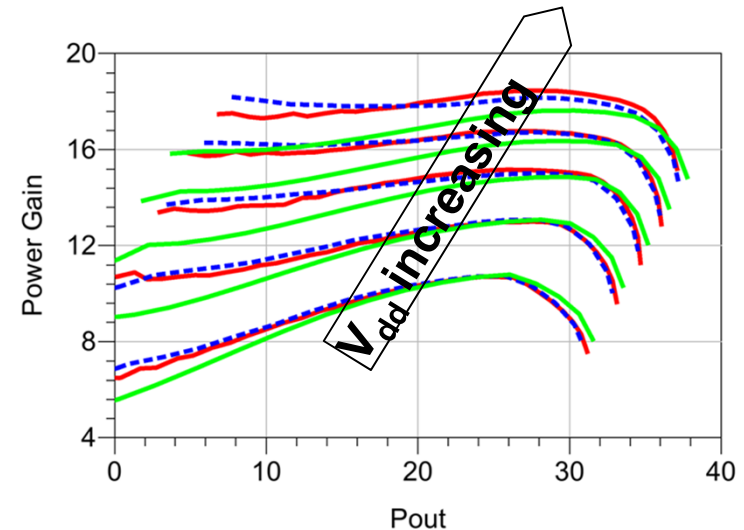
# Validation of measurement-based X-parameter model

Load-sensitivity of X-par model

## Tuner Load Set 1



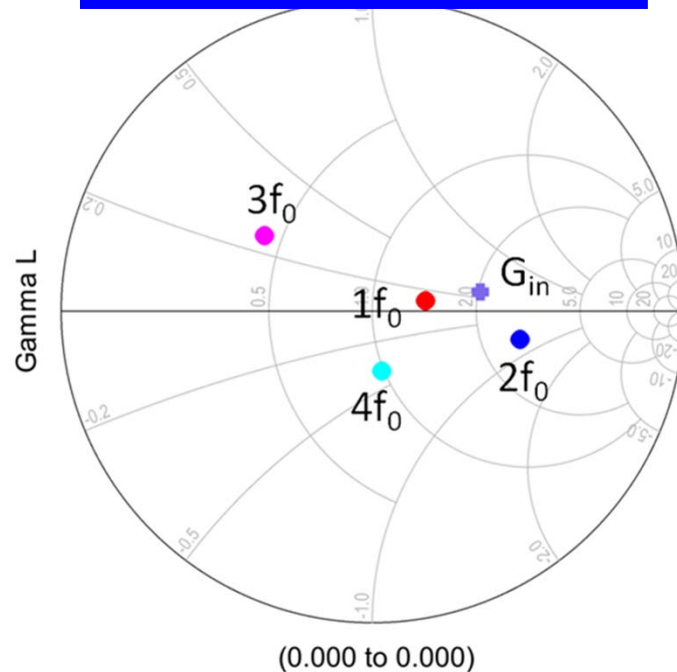
- X-parameters at 50 ohm
- Load-pull with tuner
- NVNA 50 ohm



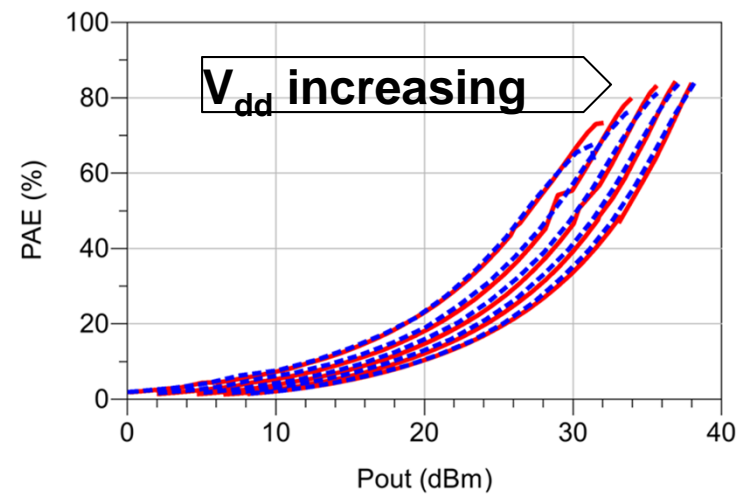
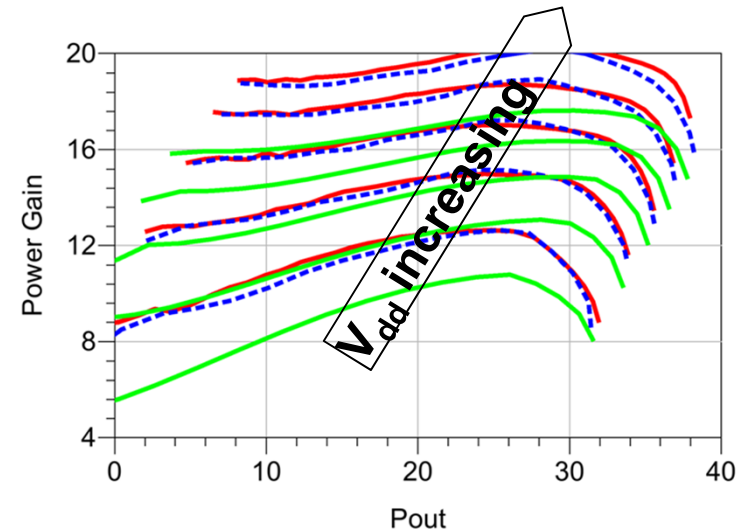


# Validation of measurement-based X-parameter model

## Tuner Load Set 2

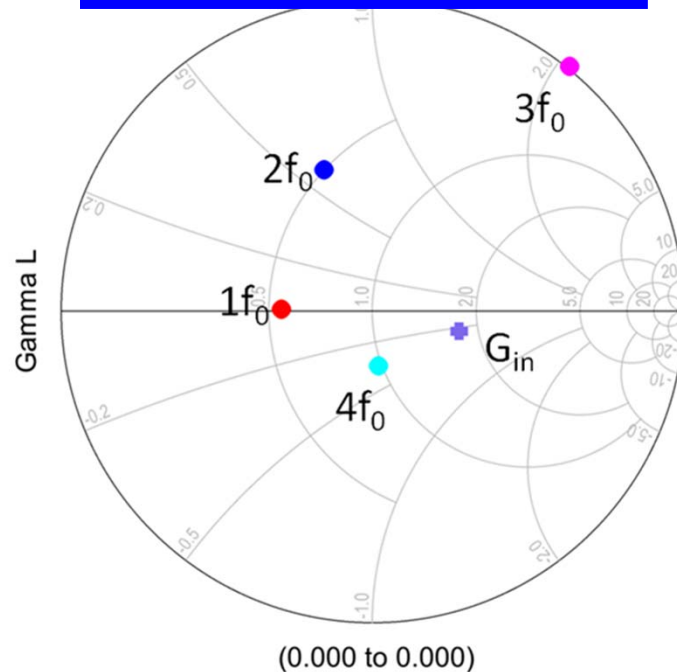


- X-parameters at 50 ohm
- Load-pull with tuner
- NVNA 50 ohm

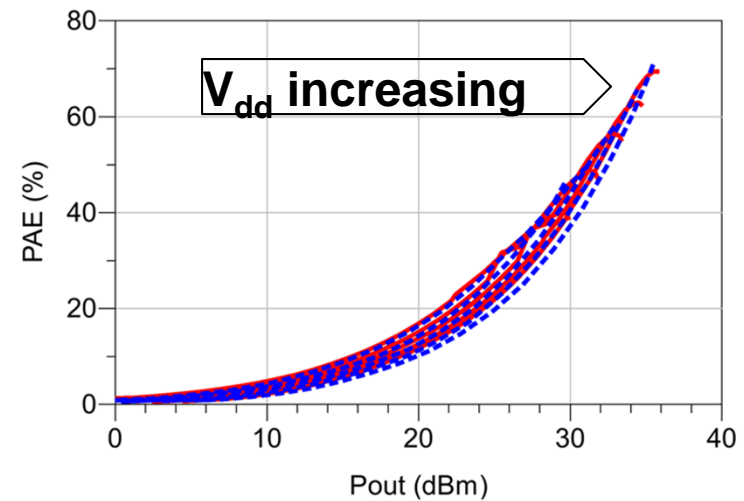
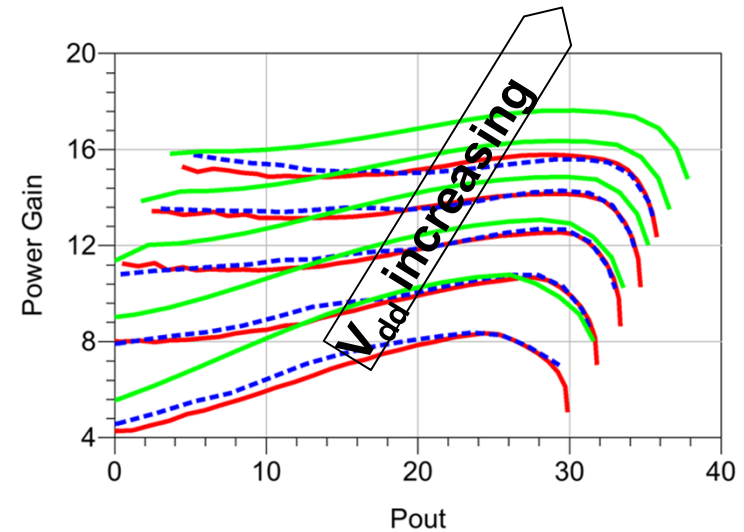


# Validation of measurement-based X-parameter model

## Tuner Load Set 3

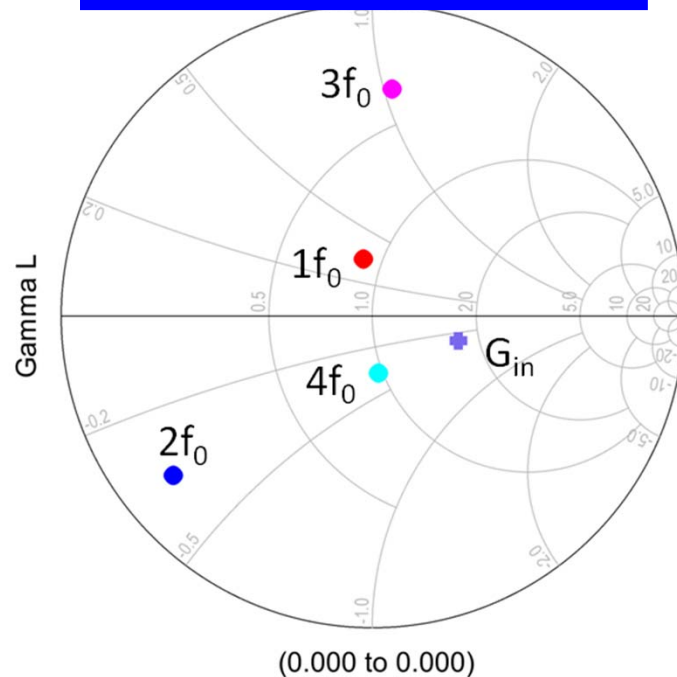


- X-parameters at 50 ohm
- Load-pull with tuner
- NVNA 50 ohm

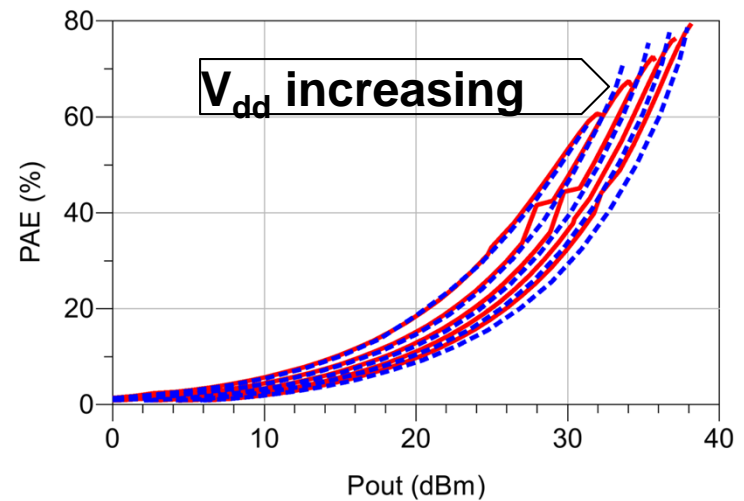
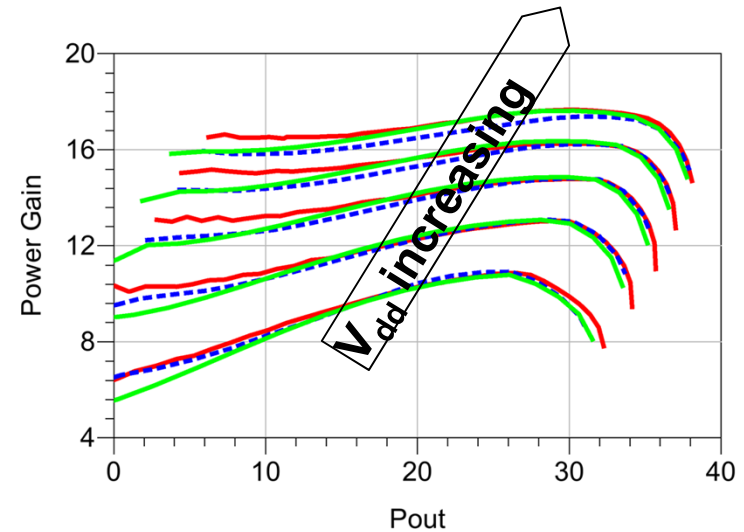


# Validation of measurement-based X-parameter model

## Tuner Load Set 4

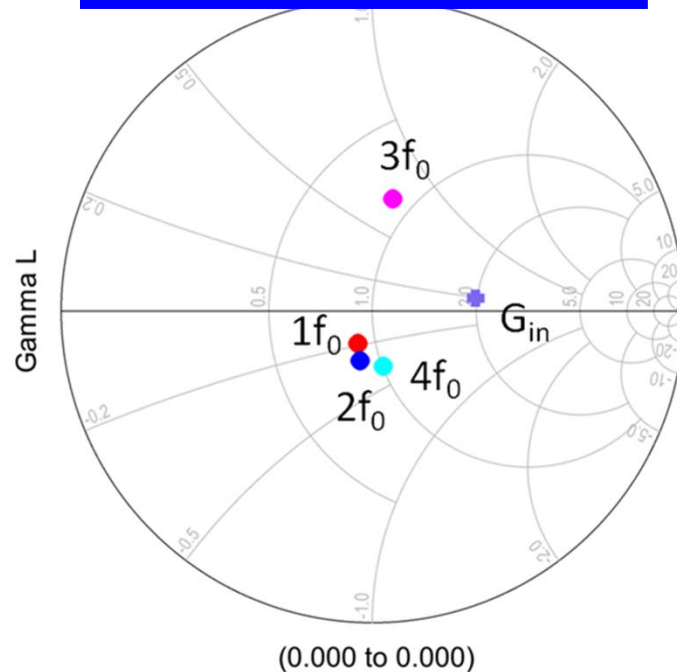


- X-parameters at 50 ohm
- Load-pull with tuner
- NVNA 50 ohm

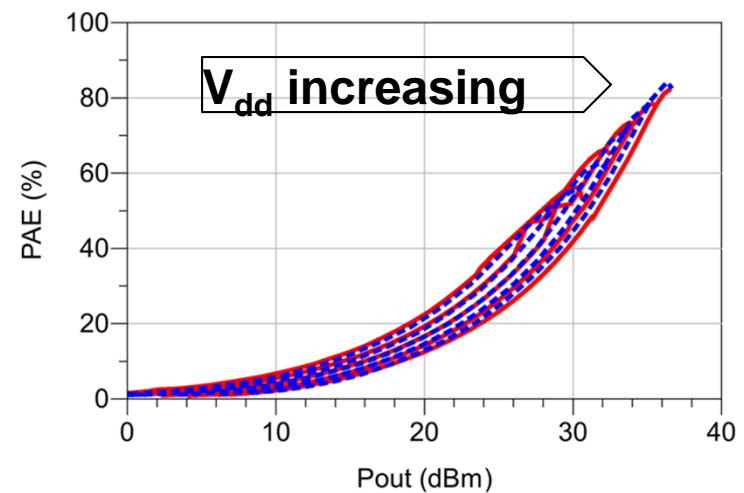
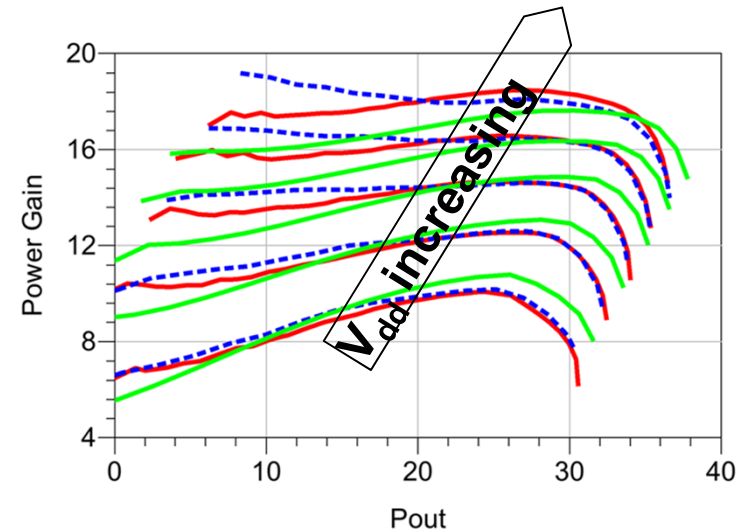


# Validation of measurement-based X-parameter model

## Tuner Load Set 5

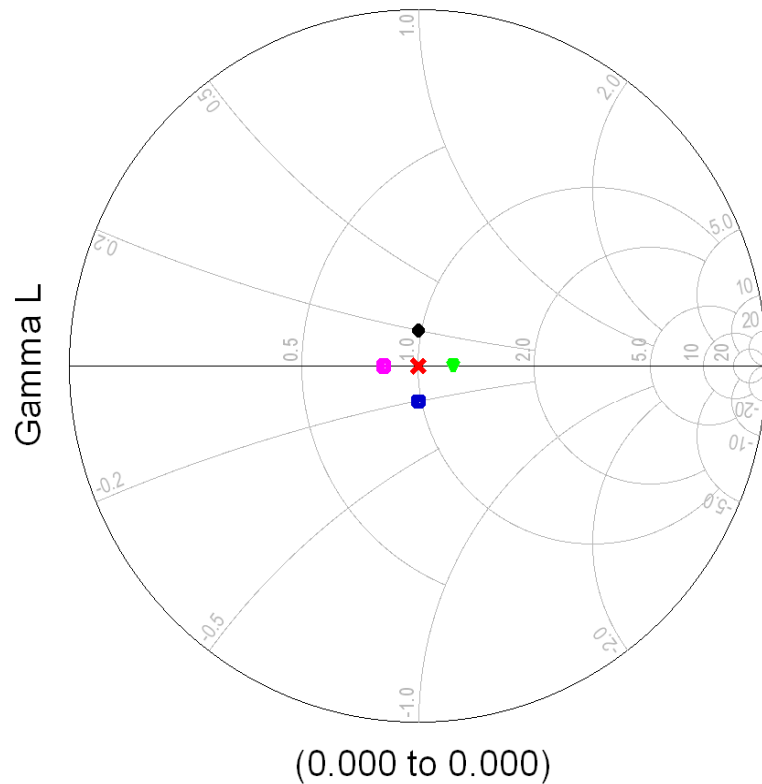


- X-parameters at 50 ohm
- Load-pull with tuner
- NVNA 50 ohm

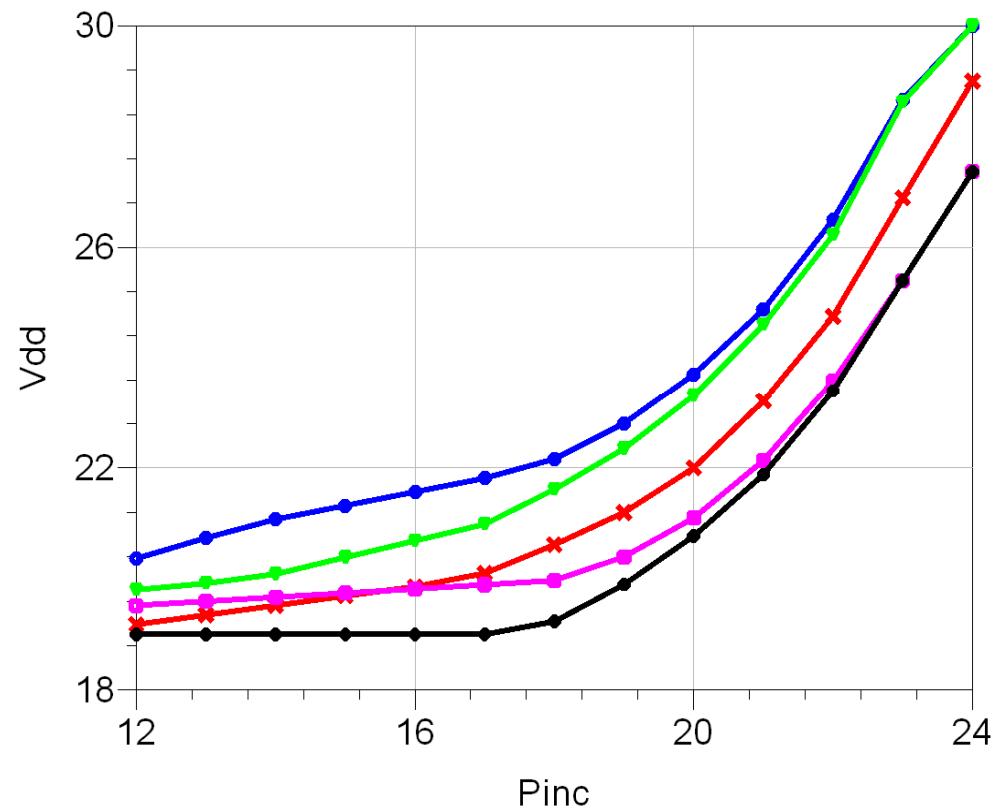


# Load-dependence of shaping table

## Loads variation

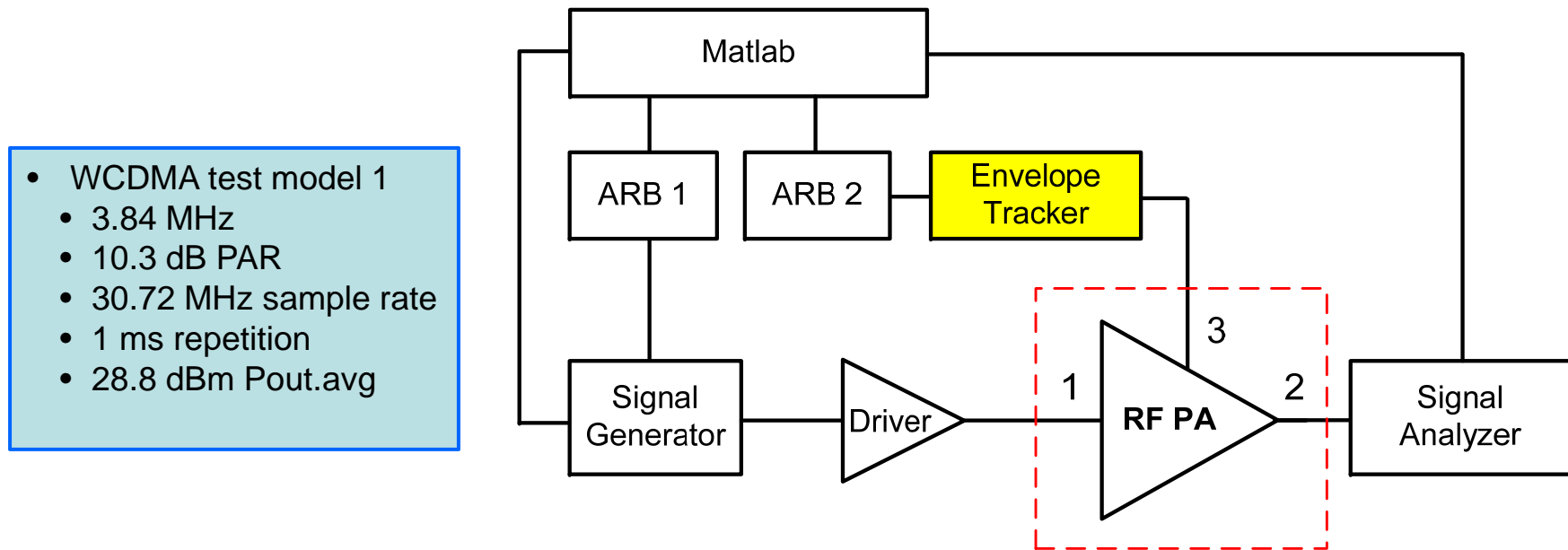


## Shaping table

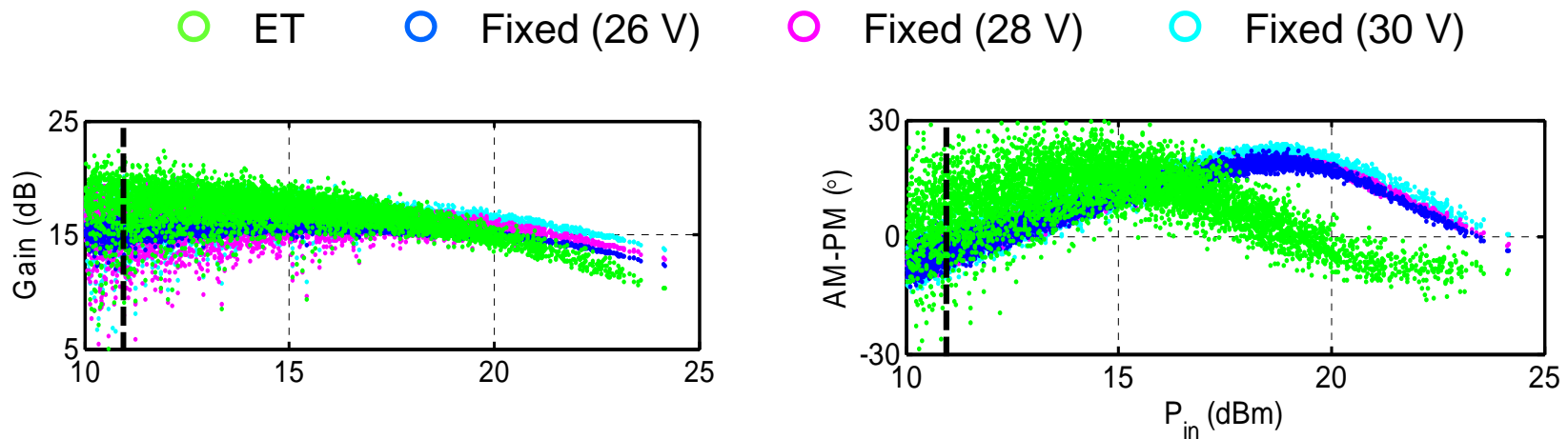


# ET measurement setup

- The WCDMA test signal was fed to the RF signal generator through arbitrary signal generator
- The shaped signal based on the XP model was fed the supply modulator through another synchronized arbitrary signal generator
- The supply modulator from [4], which has 70 MHz bandwidth and  $32 V_{\max}$ , was used for the test



# Results for GaN PA



Measured Results On GaN PA	Fixed Bias operation	ET operation
PAE	40.3%	57.8%
Output power	30.6 dBm	31.3 dBm
conditions	Averaged over 26, 28, & 30 V fixed bias conditions	21 V average bias over PDF

## Discussion

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- Static XP model based shaping table design shows significant PAE improvement under ET operation
- ET operation showed more gain compression and wider AM-PM spreading than under constant bias operation
  - lack of linearity improvement might be attributed to increased memory effects under dynamic biasing different from the ideal assumption in the simulation
  - Quasi-static assumption is likely valid when the supply modulator is ideal
  - Supply modulator output impedance and inter-connection impedance between the modulator and the PA may not be ideal
  - Slew-rate and bandwidth of the tracking amplifier are high and are not likely the problem



## Suggestions for future work

- Treat RFPA as three-terminal “incommensurate mixer” X-parameter model

$$\begin{aligned}
 B_{2,[n,m]} &= X_{2,[n,m]}^{(F)} \left( \left| A_{1,[1,0]}(t) \right|, \left| A_{3,[0,1]}(t) \right| \right) P_{1,[1,0]}^n(t) P_{3,[0,1]}^m(t) \\
 &+ \sum_{n',m',p} X_{2,[n,m];p,[n',m']}^{(S)} \left( \left| A_{1,[1,0]}(t) \right|, \left| A_{3,[0,1]}(t) \right| \right) A_{p,[n',m']} P_{1,[1,0]}^{n-n'}(t) P_{3,[0,1]}^{m-m'}(t) \\
 &+ \sum_{n',m',p} X_{2,[n,m];p,[n',m']}^{(T)} \left( \left| A_{1,[1,0]}(t) \right|, \left| A_{3,[0,1]}(t) \right| \right) A_{p,[n',m']}^* P_{1,[1,0]}^{n+n'}(t) P_{3,[0,1]}^{m+m'}(t)
 \end{aligned}$$

See talk WE3D-4 14:50-15:10 ref. [22]



## Suggestions for future work (2)

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- Application of Dynamic X-parameters to ET applications: beyond quasi-static approximation
- Characterize the modulator and take it into better account in the design

## Conclusions

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- The envelope simulation and measurement results show good quantitative agreement for the static nonlinearity of the PA versus power and drain voltage, and also as a function of load
- The load-sensitivity of the lookup table predicted by the XP model was independently validated by time-domain loadpull measurement



## Acknowledgment

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- The authors thank A. Howard, J. Horn, R. Biernacki, M. Marcu, P. Cain, A. Cognata, J. Xu, and A. Cidronali for support and valuable discussions.

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