

A Drain-Lag Model for AlGaIn/GaN Power HEMTs

O. Jardel*, F. De Groote*, C. Charbonniaud**, T. Reveyrand*, J. P. Teyssier*, R. Quéré*, D. Floriot***

*XLIM C²S² - UMR CNRS 6172, Université de Limoges, 7 rue Jules Vallès, 19100 Brive, France

**AMCAD Engineering, ESTER Technopole, BP 6915, 87069 Limoges, France

***ALCATEL-THALES III-V Lab/MITIC, route de Nozay, 91460 Marcoussis, France

Abstract — A circuit modeling drain-lag effects has been added in a non-linear electrothermal model for AlGaIn/GaN HEMTs. Modeling these trapping effects allows a better description of the I-V characteristics of measured devices as well as their large-signal characteristics. This drain-lag model is well suited to preserve the convergence capabilities and the simulation times of the non linear models of these devices. This paper presents our drain-lag modeling approach, the implementation of the model in CAD software, its operating mode, and also the parameters extraction from measurements. Then, significant comparison results will be reported on pulsed IV and large signal measurements with an AlGaIn/GaN HEMT transistor.

Index Terms — AlGaIn/GaN HEMTs modeling, Drain-lag, Trapping effects.

I. INTRODUCTION

Recently, some foundries began to commercialize AlGaIn/GaN HEMTs, showing excellent performances for high power and high frequencies applications, thanks to their very high breakdown voltages and their high sheet carrier densities.

But these components, presenting on one hand free surfaces located a few nanometers above the channel and having on the other hand no additional doping, are very sensitive to the trapping effects. Some techniques, like surface passivation, have been found or borrowed to the GaAs HEMT and MESFET technologies to reduce the impact of these traps. But some trapping effects, originating in inherent material characteristics like lattice mismatches -at the origin of dislocations- are more difficult to reduce.

The gate-lag effects are attributed to the surface traps and the drain-lag effects to buffer or substrate traps [1][2]. Many measurements validated this point: techniques of surfaces passivations are now very efficient and we can notice that gate-lag effects are quasi-removed on the up to date devices. Nevertheless, drain-lag effects represent a big issue, as they imply current transients harmful to power and linearity characteristics.

However, there is a need for non-linear models of these devices, and hence some solutions have been proposed to deal with modeling dispersion effects on transconductance and on output characteristics in FETs [3][4][5] due to drain-lag effects during transient simulations. The circuit presented here takes into account these effects but also separates the capture and emission process, which leads to a better description of the

pulsed IV and large signal characteristics obtained by harmonic balance simulations. Our method also enables an easy implementation in CAD software, and preserves the convergence capabilities and the simulation times of the devices non-linear models.

II. DESCRIPTION OF THE DRAIN LAG EFFECTS

The term “drain-lag” is used to describe the slow transient response of the drain current when the drain-source voltage is pulsed.

When the voltage within the pulse is higher than the quiescent bias point one, the traps capture free charges. This phenomenon is very fast, compared to the typical lengths of the pulses.

When the voltage within the pulse is lower than the quiescent bias point, the traps release their charges. The process duration can be very large (about a few seconds in some cases).

As free carriers are captured or released, they do not take part to the output current instantaneously. This phenomenon is at the origin of current transients, as illustrated on the fig. 1, and induces a dispersion of the devices power characteristics.

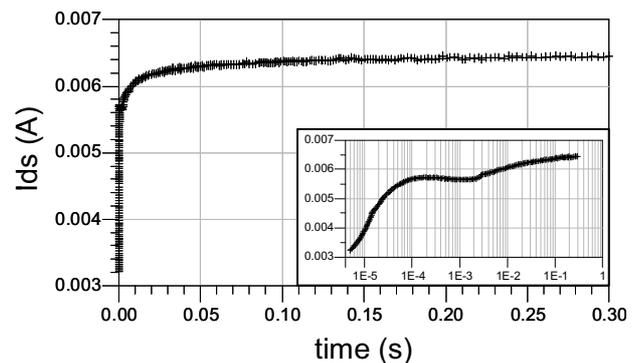


Fig. 1. Evidence of drain-lag phenomenon on a 0.6 mm AlGaIn/GaN HEMT. V_{gs} is kept at a fixed value equal to -6V, whereas V_{ds} is pulsed from 30 to 20V. Self-heating effects are negligible in this case.

Each trap level adds an exponential contribution to the current transient. Fitting this current transient would require at least 6

exponential terms, i.e. as many as trapping levels. Our model adds these exponential terms thanks to RC cells.

III. CIRCUIT DESCRIPTION

Drain-lag effects can be considered as self-backgating effects, as they are caused by deep traps beneath the channel: the space charge area created by these traps acts as a virtual gate by constricting it, and so adds a contribution to pinch the transistor off [6][7]. Hence, the drain voltage transients are equivalent to a virtual gate voltage transient and a fortiori to a gate-source voltage transient. We will use this analogy in our model.

A one-trap drain-lag model schematic is given at fig 2.

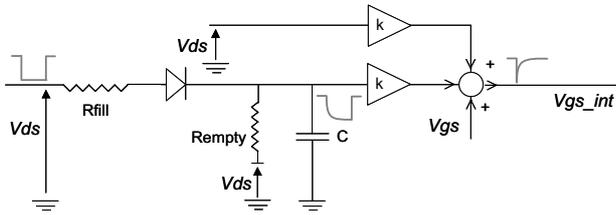


Fig. 2. Schematic of the drain lag model.

This circuit works as an envelope detector. There are two input voltages: V_{gs} and V_{ds} ; and one output voltage, named V_{gs_int} , which becomes the command voltage of the current source. The diodes have a threshold voltage of 0 Volt.

In the case where V_{ds} increases, the diode is opened, and the capacitance C charges through the resistance R_{fill} . The time constant associated to the filling of the trap is given by:

$$\tau_{fill} \approx R_{fill} \cdot C, \quad (\text{as } R_{empty} \gg R_{fill}) \quad (1)$$

When V_{ds} decreases, the diode blocks and the capacitance C discharges through the resistance R_{empty} . The release time constant is given by:

$$\tau_{empty} = R_{empty} \cdot C \quad (2)$$

The density of each trap is directly linked to the amplitude of the transient it creates. The relative amplitude of the trap number n (i.e. if we normalize steady-state current value to 1) is noted k_{rel_n} . Each k_{rel_n} has to be multiplied by the total drain current there would be at steady state or if there were no traps to obtain the absolute amplitude of the trap transient k_n . This current is expressed as a linear function of V_{gs} for reasons of simplicity:

$$I_d = Gm_{DC} \cdot (V_{gs} - V_{pinch-off}) \quad (3)$$

Thus, we have:

$$k_n = k_{rel_n} \cdot Gm_{DC} \cdot (V_{gs} - V_{pinch-off}) \quad (4)$$

but the equation we exactly use is :

$$k_n = k_{rel_n} \cdot Gm_{DC} \cdot \left(\left(\text{above}(V_{gs}, 0.1, -V_{pinch-off}) - V_{pinch-off} \right) \right) \quad (5)$$

The function above works in the following way:

$$\text{If } V_{gs} < V_{pinch-off}, \text{ then } V_{gs} = V_{pinch-off} \text{ else } V_{gs} \quad (6)$$

The smooth transition between the two slopes is tuned by the second parameter (here equal to 0.1). An equation based on a tanh can also be used. The form of k_n is showed at fig 3.

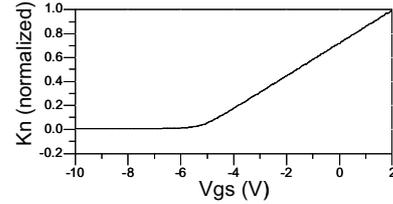


Fig. 3. Model parameter : k_n versus v_{gs} .

IV. PARAMETERS EXTRACTION

In our example of fig.1, we can obtain a fairly adequate fit with only two time constants, as it is showed on fig 4, and thus we have implemented a drain lag circuit with two traps. As the dependence in temperature of time constants of the traps is not considered here, the measurements were performed at the estimated temperature of work of the device in its spotted application.

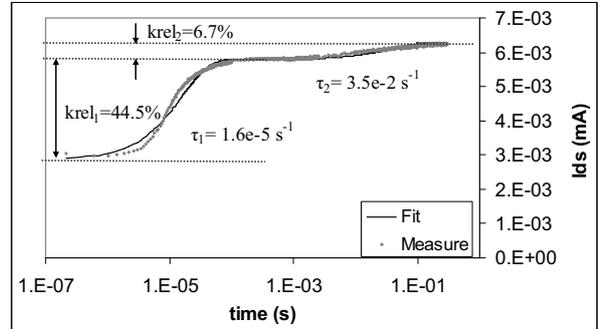


Fig. 4. Approximate fit of a current transient due to drain-lag effects on a $8 \times 75 \mu\text{m}$ device. We obtain the relative amplitudes and the time constants of the traps.

From this measured curve, we obtain the couples of parameters describing each one a trap: $(\tau_1, krel1)$ and $(\tau_2, krel2)$, where the terms τ_n represent the emission time constants.

The parameter Gm_{DC} in (3) is obtained from DC IV curves (at low V_{ds} to limit thermal reduction of Gm_{DC}) or pulsed IV curves with a quiescent bias point of $V_{ds0}=0V$, i.e. when trapping effects do not appear (see paragraph V).

The R_{fill} value is fixed at a small value, as we consider that the filling of the traps is very fast (< 50 ns).

V. PULSED I-V CHARACTERIZATION OF THE TRANSISTOR

A. Measurements description

In order to characterize the traps, pulsed IV measurements were performed at ambient temperature. The choice of the quiescent bias point allows to observe the trapping effects on the output current and even to discern gate-lag from drain-lag effects. The method has already been described in [8]. We can focus on three configurations:

1) If the quiescent bias point is $V_{gs0}=0$ V and $V_{ds0}=0$ V, the classical IV curves measurement implies that V_{gs} is pulsed down and V_{ds} is pulsed up. Hence, both gate- and drain-lag related traps are filling.

Considering that the filling of the traps is very fast compared to pulses duration, the traps state is that of the bias during pulse.

2) If the quiescent bias point is, for example, $V_{gs0}=-6$ V (when the device is pinched-off) and $V_{ds0}=0$ V, the gate source and the drain source voltages are pulsed up during the measurement. Hence, the traps commanded by gate-source voltage are filling (fast), and the traps commanded by drain-source voltage are emptying (slowly). We can conclude that inside the pulse, the traps commanded by gate-source voltage remain in the same state they had at quiescent bias point, and the traps commanded by the drain-source voltage have changed state and are now in the state of the pulse bias.

3) If the quiescent bias point is, for example, $V_{gs0}=-6$ V (pinched-off) and $V_{ds0}=25$ V, the drain source voltage is pulsed down for the measurement points where $V_{ds} < 25$ V and pulsed up for $V_{ds} > 25$ V.

Considering that the traps discharge is very slow compared to the duration of the pulses, the traps state inside a pulse is that of the quiescent bias point for $V_{ds} < 25$ V.

Note that we took care of maintaining the output current equal to 0 A. at quiescent bias points and that we chose the length of the pulses as short as possible to avoid thermal effects and their influence on output current.

These measurements allow us to discriminate traps and even gate- from drain-lag related traps: by comparing the measurement described in 1) with the measurement described in 2), we note that only gate bias changed and thus we observe the influence of gate-lag effects.

By comparing 2) with 3), only the drain bias changed and we observe the influence of drain-lag effects.

The IV networks showed fig.5 were measured on a $2 \times 50 \mu\text{m}$ AlGaIn/GaN HEMT. On the first graph are superimposed two IV Networks corresponding to cases 1) and 2) and showing that gate-lag effects. On the second graph are compared cases 2) and 3) showing drain-lag effects.

This device has negligible gate-lag effects, which shows that the passivation layer is very efficient, but the drain-lag effects are important, inducing a large drain current dispersion and a knee voltage increasing.

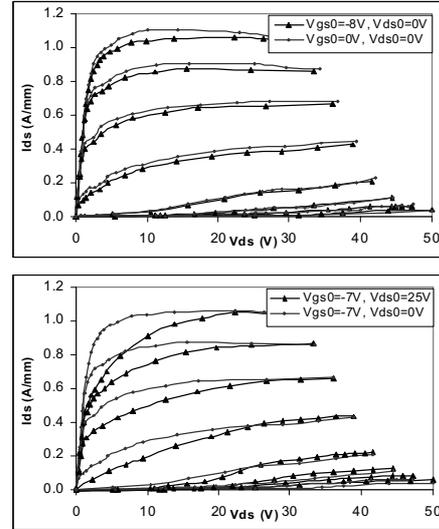


Fig. 5. Pulsed IV measurements at different quiescent bias points of a $2 \times 50 \mu\text{m}$ AlGaIn/GaN HEMT (pulses length: 350 ns, period: $30 \mu\text{s}$, V_{gs} from -7 to 0V).

VI. MODEL VALIDATION ON PULSED I-V AND LARGE SIGNAL MEASUREMENTS

The AlGaIn/GaN HEMT model used here has already been presented in [9]. However, the drain-lag subcircuit we present here could be implemented in any model, as it just impacts on the gate-source voltage at the input of the current source.

A. I-V simulations

Fig. 6 shows the influence of the trapping effects on pulsed IV characteristics. Measurements corresponding to case 3) are first compared to pulsed IV simulations at the same quiescent bias point, and then to simulations at a bias point corresponding to case 1). This latter case corresponds to the results we would obtain for all the quiescent bias points if the trapping model were inactivated.

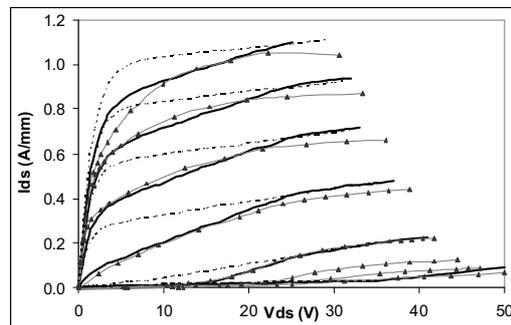


Fig. 6. Pulsed IV measurements for V_{gs} from -7 to 0 V at a quiescent bias point of $V_{gs0}=-7$ V and $V_{ds0}=25$ V (lines with tics), pulsed simulations in the same conditions (continuous lines), and for a quiescent bias point of $V_{gs0}=0$ V, $V_{ds0}=0$ V (dashed lines).

We can remark that the trapping model allows reproducing the current dispersion and the knee voltage increase due to drain-lag effects. The large decreases of the load cycles excursions during large signal operations induced by these phenomena have a significant influence on power characteristics. Thus, it is very important to reproduce them well, as we can see in the following chapter.

B. Large signal simulations

The modeled device is an $8 \times 75 \mu\text{m}$ AlGaIn/GaN HEMT on SiC substrate from Thalès-Tiger. The model is electrothermal, and was extracted from pulsed I-V and [S]-parameters measurements. Load-Pull measurements are performed at 25 V in class AB at 10 GHz for an optimum load impedance of $20.3 + j29.6$ Ohms. The measured and simulated (with and without drain-lag modeling) large-signal characteristics are showed fig.7.

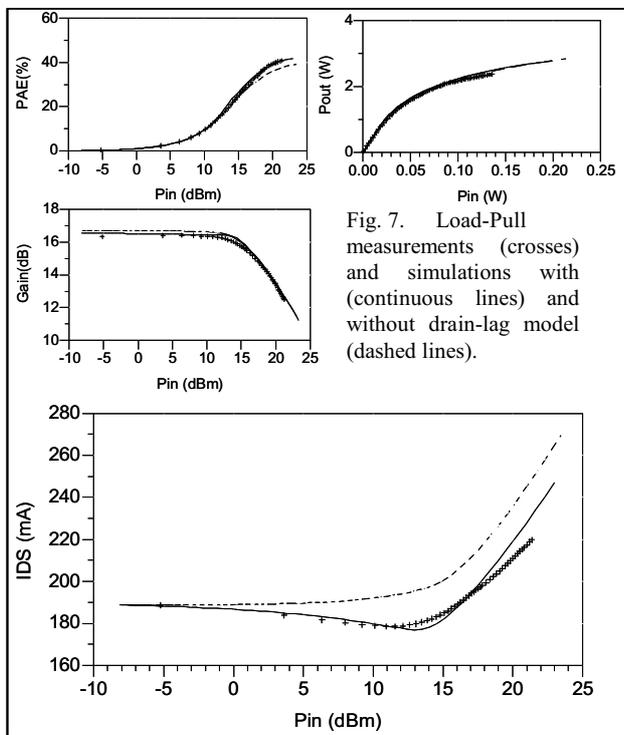


Fig. 7. Load-Pull measurements (crosses) and simulations with (continuous lines) and without drain-lag model (dashed lines).

What is to notice is that the measured DC output current decreases when the input power increases and increases after (when power saturation begins). This phenomenon is impossible to fit without the drain-lag model, which leads to an important error on this parameter. Drain-lag effects also induce a decrease of the output power and the gain. The PAE is increased and hence better fitted as it directly depends on the DC output current. Broadly, the power characteristics are better reproduced.

VII. CONCLUSION

A subcircuit modeling drain-lag by modifying the gate-source voltage at the input of the current source was presented. A very similar circuit can be used for gate-lag modeling by replacing the V_{ds} dependence by a V_{gs} one, inverting the diodes terminals and choosing negative traps amplitudes. The latter circuit can be useful when devices present strong gate-lag effects, inducing a slower increase of the DC component of the drain current at the compression.

This circuit can be implemented on HEMTs and even MESFETs models. Its simplicity allows extracting quite fast the circuit parameters, with a few measurements.

ACKNOWLEDGEMENT

The authors wish to acknowledge the EDA (European Defence Agency) for the financial support in the context of the KORRIGAN Workpackage 3.3 (RTP 102.052).

REFERENCES

- [1] W. Mickanin, P. Canfield, E. Finchem, B. Odekirk, "Frequency dependent transients in GaAs MESFETs: process, geometry, and material effects", GaAs IC Symp. Dig., 1989, pp. 211-214.
- [2] J.C. Huang et al., "An AlGaAs/InGaAs pseudomorphic high electron mobility transistor with improved breakdown voltage for X- and Ku-band power applications", IEEE Trans. on Microwave Theory and Techniques, vol. 41, pp. 752-759, 1993.
- [3] T.J. Brazil, "A universal large-signal equivalent circuit for GaAs MESFET", in Proc. 21st EUMC, Stuttgart, Germany, 1991, pp 921-926.
- [4] C. Camacho-Penalosa, C.S. Aitchison, "Modeling frequency dependence of output impedance of a microwave MESFET at low frequencies", Electron. Lett., vol. 21, no 12, pp 528-529, 1985.
- [5] M.S. Shirokov, R.E. Leoni, III, J. Bao, J.C.M. Hwang, "A Transient SPICE Model for Digitally Modulated RF Characteristics of Ion-Implanted GaAs MESFETs", IEEE Transactions on Electron Devices, vol. 47, no 8, Aug. 2000.
- [6] K. Horio, Y. Fuseya, "Two-dimensional simulations of drain-current transients in GaAs MESFET's with semi-insulating substrates compensated by deep levels." IEEE Transactions on Electron Devices, vol.41, no.8, Aug. 1994, pp.1340-1346.
- [7] Z. Ouarch, J.M. Collantes, J.P. Teyssier, R. Quéré, "Measurement based nonlinear electrothermal modeling of GaAs FET with dynamical trapping effects," Microwave Symposium Digest, 1998 IEEE MTT-S International, vol.2, no.pp.599-602 vol.2, 7-12 Jun 1998.
- [8] C. Charbonniaud, S. De Meyer, R. Quéré, J.P. Teyssier, "Electrothermal and Trapping Effects Characterization", GAAS 2003, 6-7 Oct, 2003 Munich.
- [9] S. Forestier, T. Gasseling, P. Bouysse, R. Quéré, J.M. Nebus, "A new nonlinear capacitance model of millimeter wave power PHEMT for accurate AM/AM-AM/PM simulations", IEEE Microwave and Wireless Components Letters, vol.14, no.1, Jan. 2004, pp. 43-45.

A Drain-Lag Model for AlGaIn/GaN Power HEMTs

O. Jardel, F. De Groote, C. Charbonniaud, T. Reveyrand,
J. P. Teyssier, R. Quéré, D. Floriot



XLIM-C²S²/MITIC 7, rue Jules Vallès, 19100 Brive, France

Outline

Presentation of a sub-circuit modeling drain-lag (and also gate-lag) effects especially for AlGaN/GaN HEMTs non-linear models

- 1) Origins and impacts of trapping effect on transistors performances
- 2) Description of the sub-circuit modeling traps and the procedure of extraction of the parameters
- 3) Validation (Pulsed-IV, Load-Pull, LSNA) of a large-signal model including trapping effects

Motivation

- Lag effects are difficult to remove (especially drain-lag), and have harmful consequences on electrical performances of devices
- Large-signal models of transistors without trapping effects can't reproduce well large-signal characteristics, especially for several load impedances.

Pros & Cons

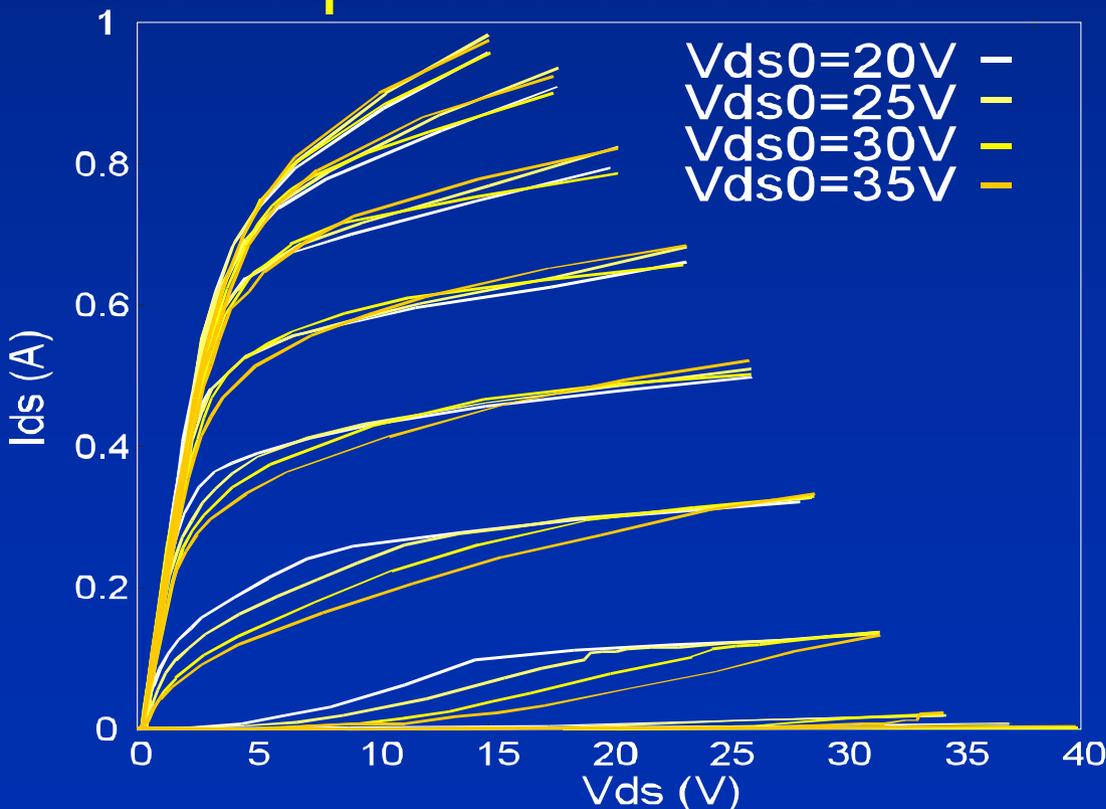
- **++** Better description of the large-signal characteristics in function of the voltages excursions and the frequencies
- **-** Adds little complexity to the transistor model, and to the extraction procedure.
- **-** Simulation time slightly increased

➔ Designed to be easy to implement and to extract...

... simplifications to describe the trapping effects

The drain-lag phenomenon

- **Origins:** Attributed to buffer defects (lattice mismatches, dislocations, doping...)
- **Impact :** electrical anomalies – ex: dispersion of pulsed-IV characteristics versus quiescent V_{ds} bias and pulses durations

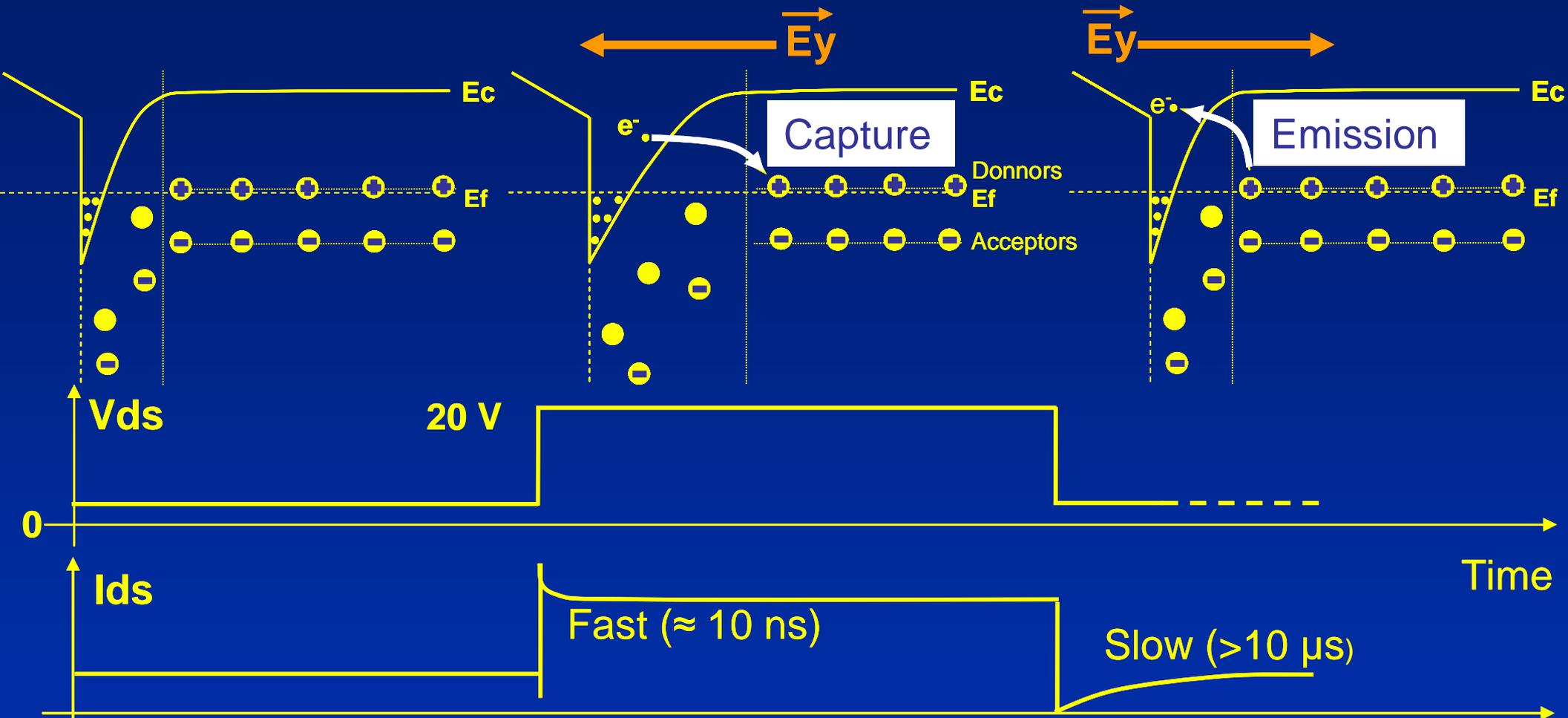


~~$I_d = f(V_{gs}, V_{ds})$~~

↓ **Traps**

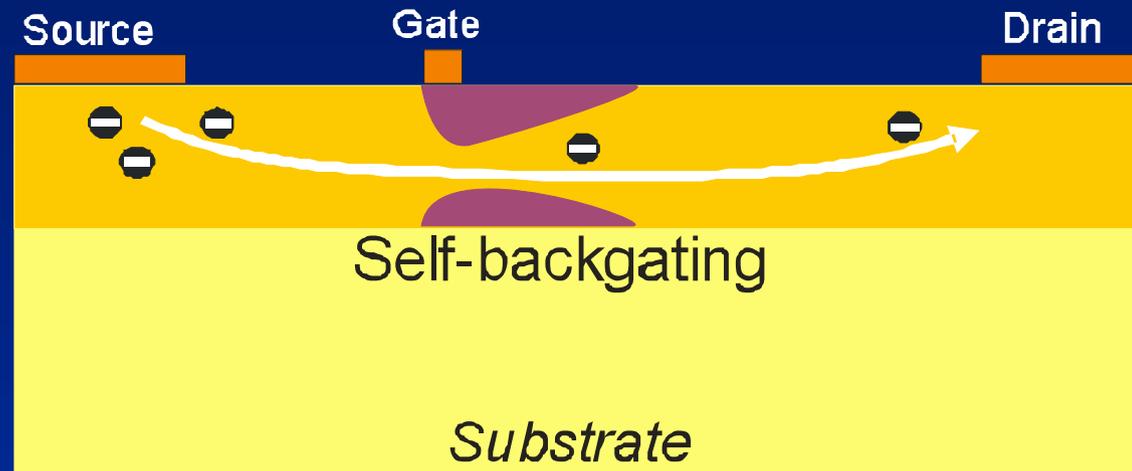
$I_d = f(V_{gs}, V_{ds}, V_{bias}, \text{time})$

Bands point of view



- Some charges don't participate to output current
- Asymmetric behavior of capture and emission times
→ **Electrical performances decrease**

Modeling drain-lag: analogy with MESFET's self-backgating (1/2)



- MESFETs: charged traps at channel/substrate interface acts like a virtual gate
 - constricts the channel and decrease I_{ds} (similar to a V_{gs} change)
- HEMTs: Traps capture free charges → decrease I_{ds} ...

Modeling drain-lag: analogy with MESFET's self-backgating (2/2)

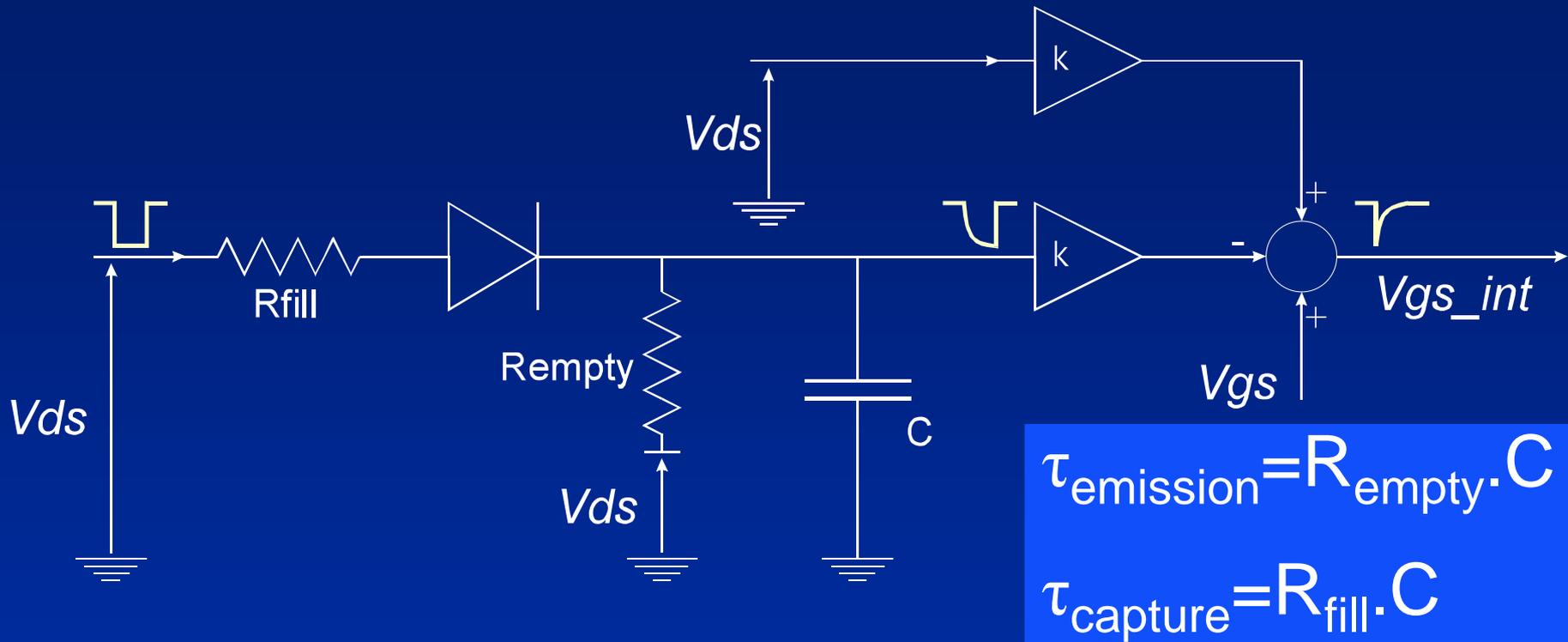
$$I_{ds} = f(V_{gs}, V_{ds}, V_{ds_bias}, t)$$



$$I_{ds} = f(V_{gs_trap}(V_{ds_bias}, t), V_{ds})$$

- Trapping effects are seen like a contribution on V_{gs}
- Do not change the current source topology, just change V_{gs} commanding the current source
- Easier to implement, can be used for different models/topologies of current sources

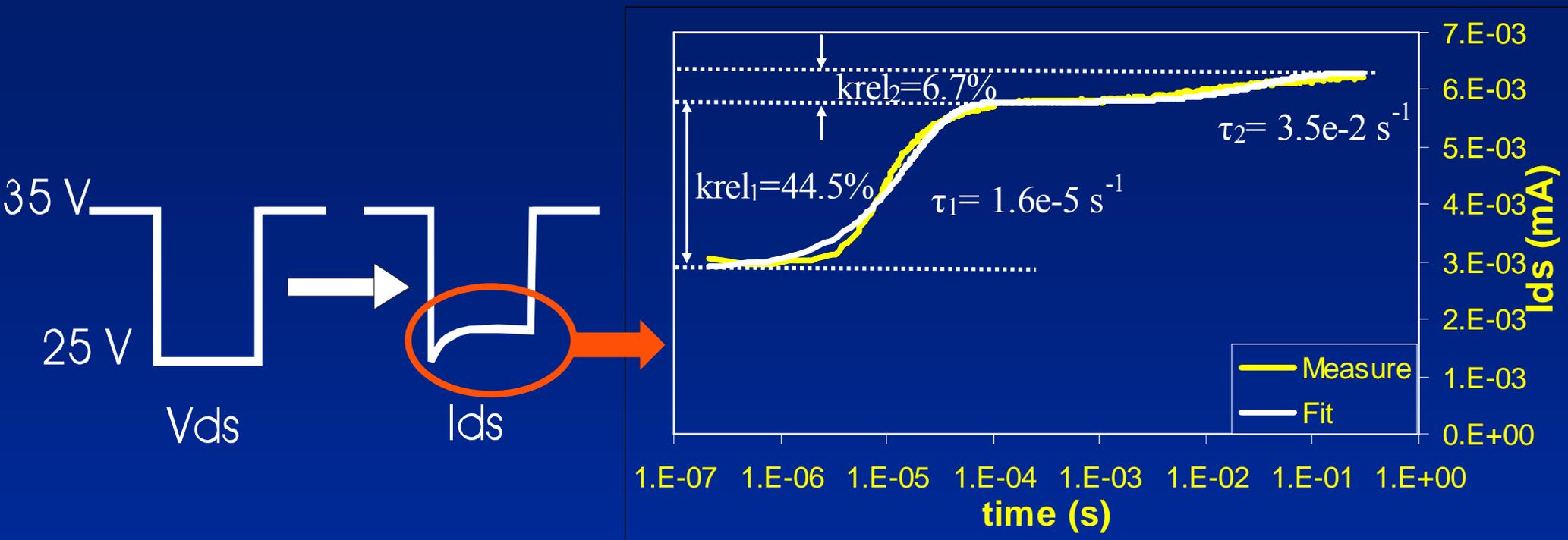
Drain-lag sub-circuit description



- Works like an envelope detector
- Number of circuits = number of traps modeled
- Only 3 parameters to extract for each trap:

Rempty, Rfill, k

Extraction of parameters (1/2)



- Current transient measurement when V_{ds} is pulsed (in order traps to release their charges)
 - Obtaining:
 - Number of modeled traps
 - Emission time constants
 - Relative amplitude of each trap

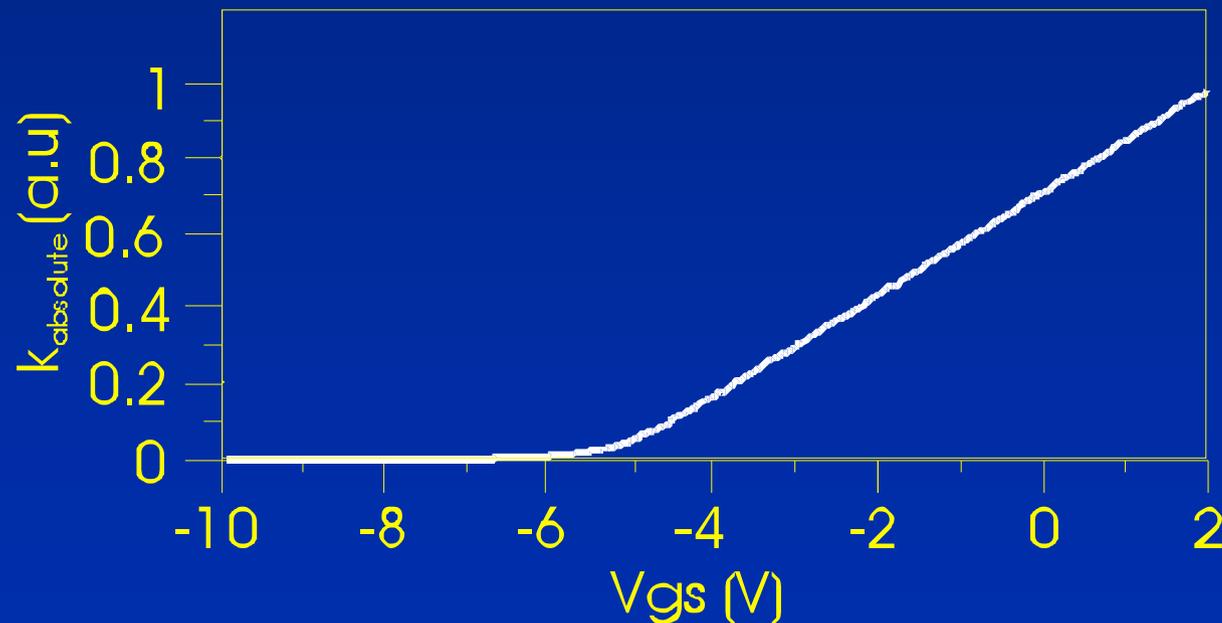


Avoid thermal effects during meas.

Extraction of parameters (2/2)

Absolute amplitude of each trap (k) =
relative amplitude (k_{REL}) \times output current

I_{ds} modeled simply as: $I_{ds} = Gm_{DC} \cdot (V_{gs} - V_{pinch-off})$

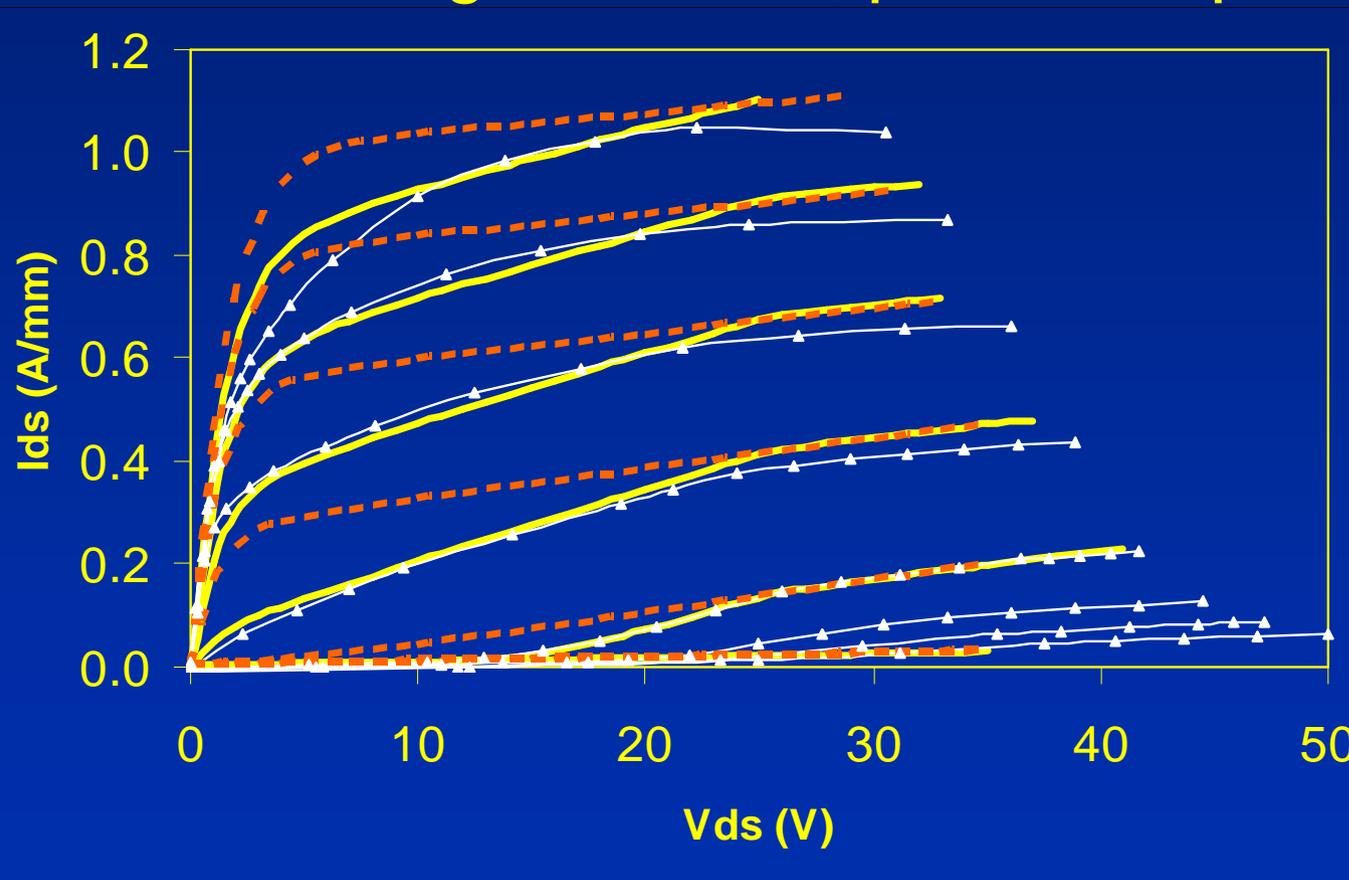


Capture time constants not measured (too fast)

→ fixed at a few nanoseconds

Model (drain-lag) validation on Pulsed-IV measurements

- Pulsed IV measurements @ $V_{ds_bias}=25V$
- Pulses length: 400 ns, period: $10\mu s$



capture < 400 ns

400 ns < émission

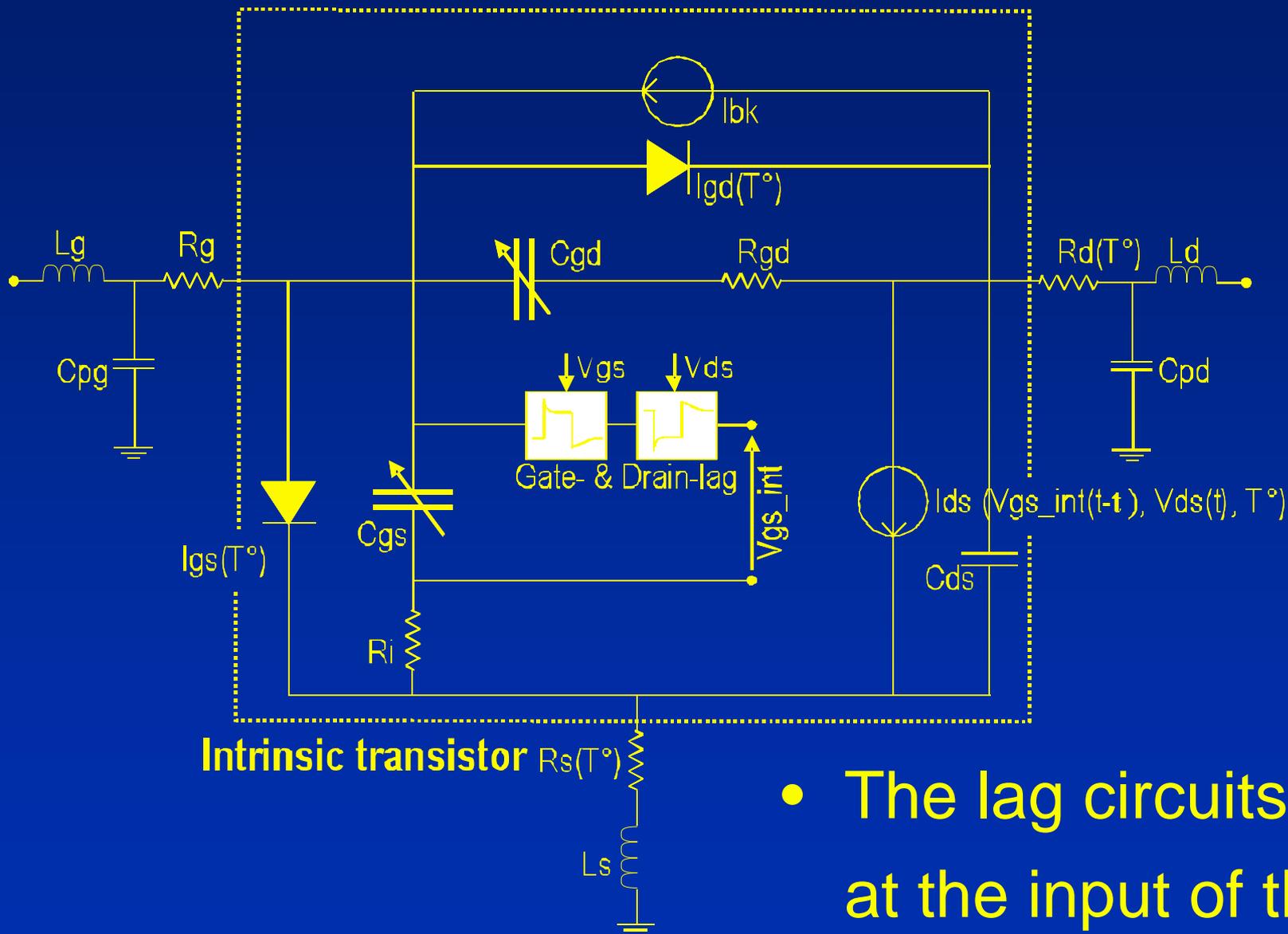
— Traps model activated
- - - Traps model inactivated
— Measurement ($V_{ds0}=25V$)

- Modeling of 1) Knee voltage increase
2) Current decrease for $V_{ds_pulse} < V_{ds_bias}$

Model of Gate-lag

- The same sub-circuit topology can be used for modeling **gate-lag** effects
 - Invert diode terminals
 - k negative

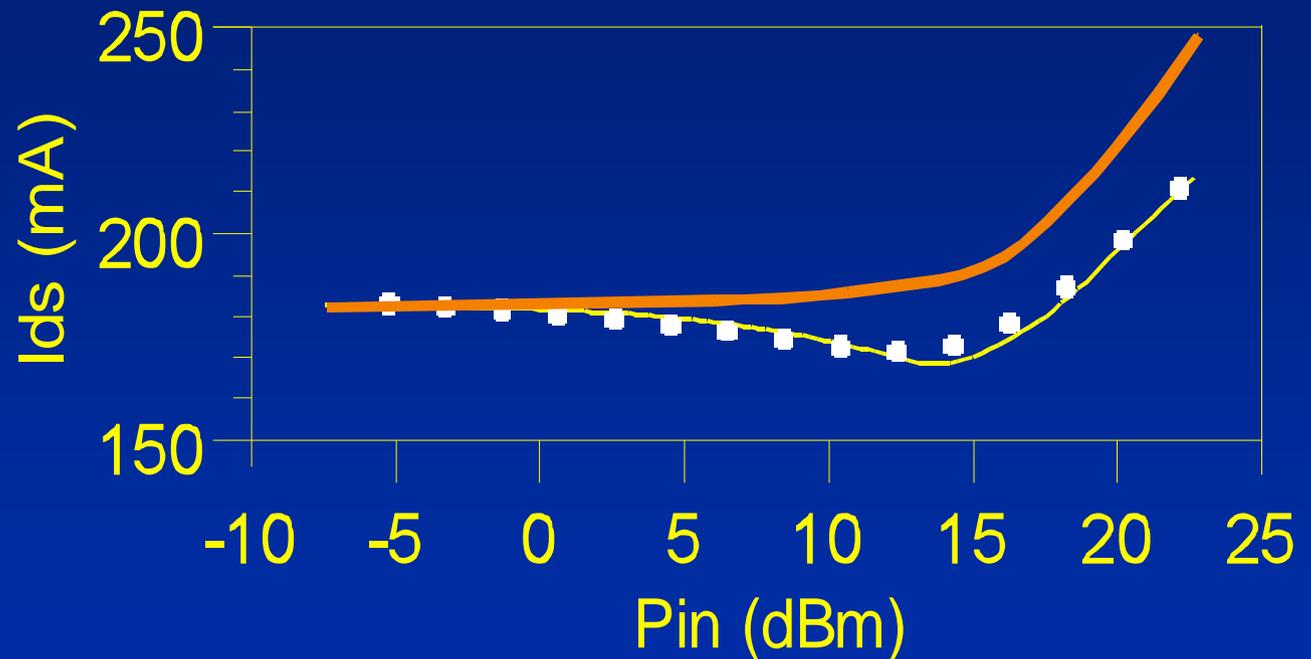
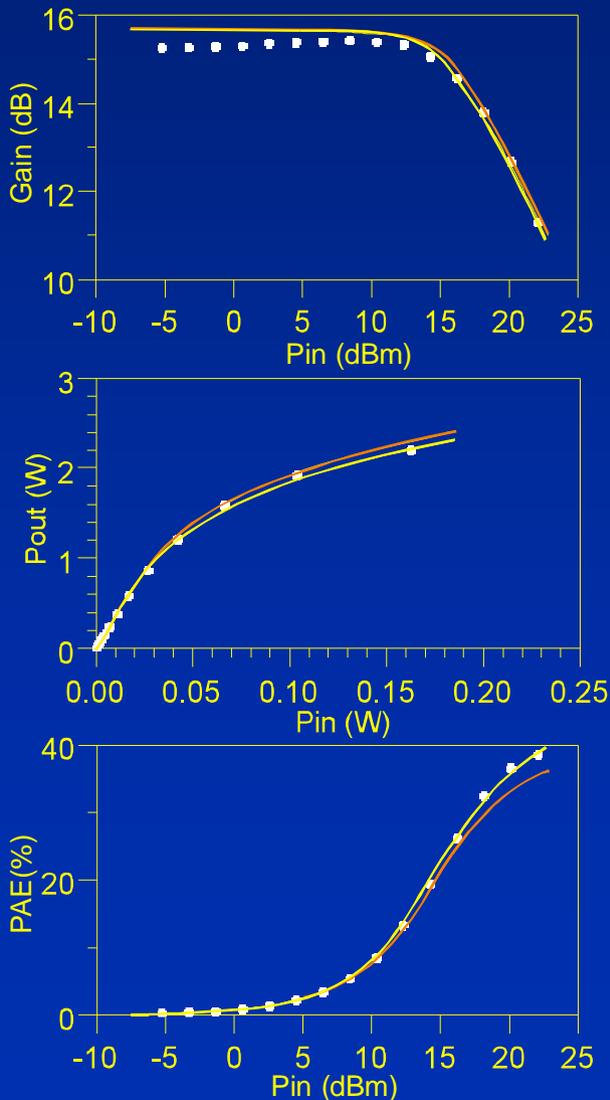
Topology of the non-linear model with gate- & drain-lag



- The lag circuits are in series at the input of the main current source

Load-pull validation @ 10 GHz

AlGaIn/GaN HEMT 8x75 μ m : Load-pull measurement on
 $Z_{opt}=20.3+j29.6$ (DC/CW) class AB (25V, 180mA)



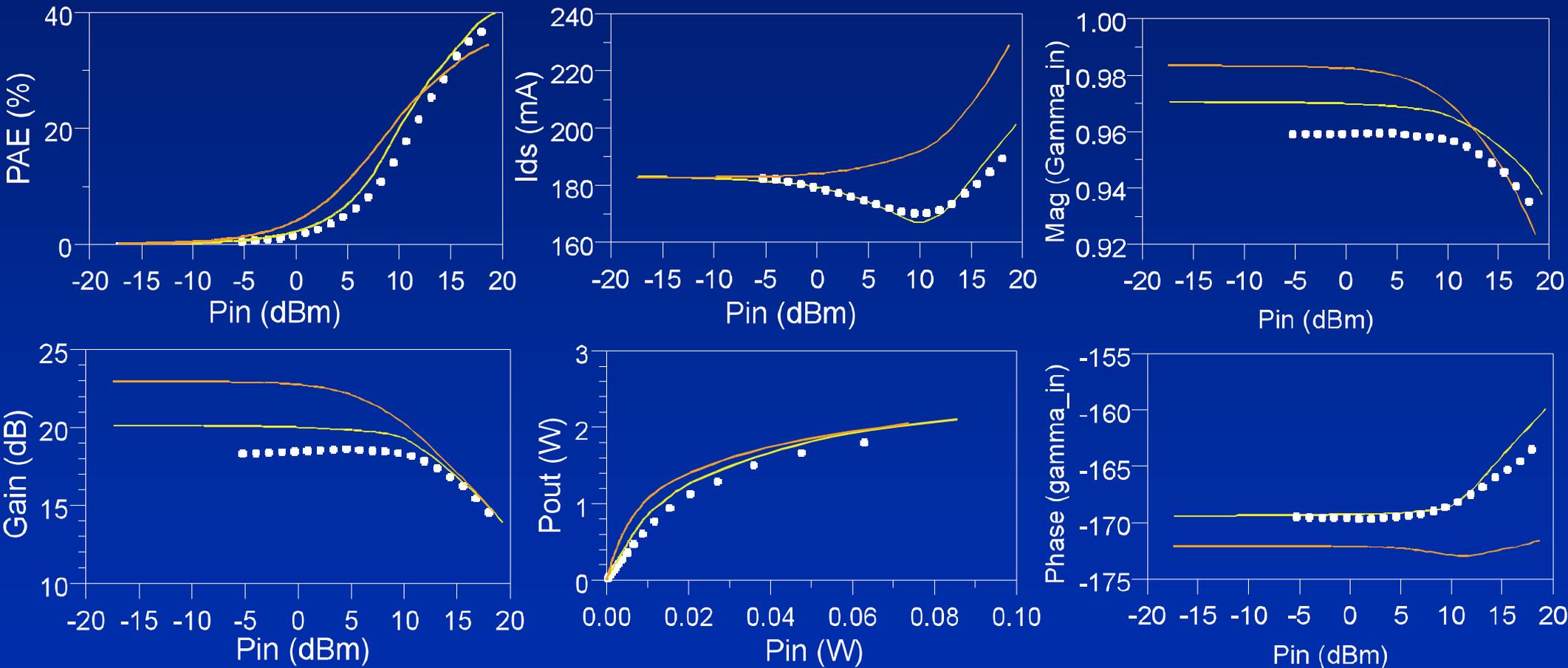
- Decreasing form of the mean output current only reproduced with traps modeled

→ PAE better reproduced

Load-pull validation @ 10 GHz

Impact of traps modeling on simulations on high VSWR

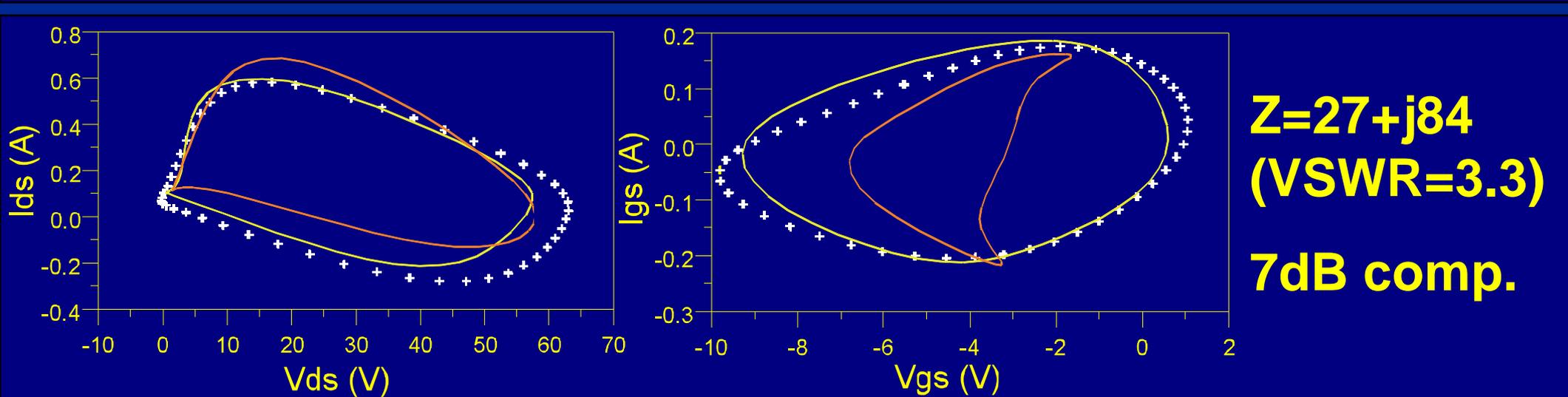
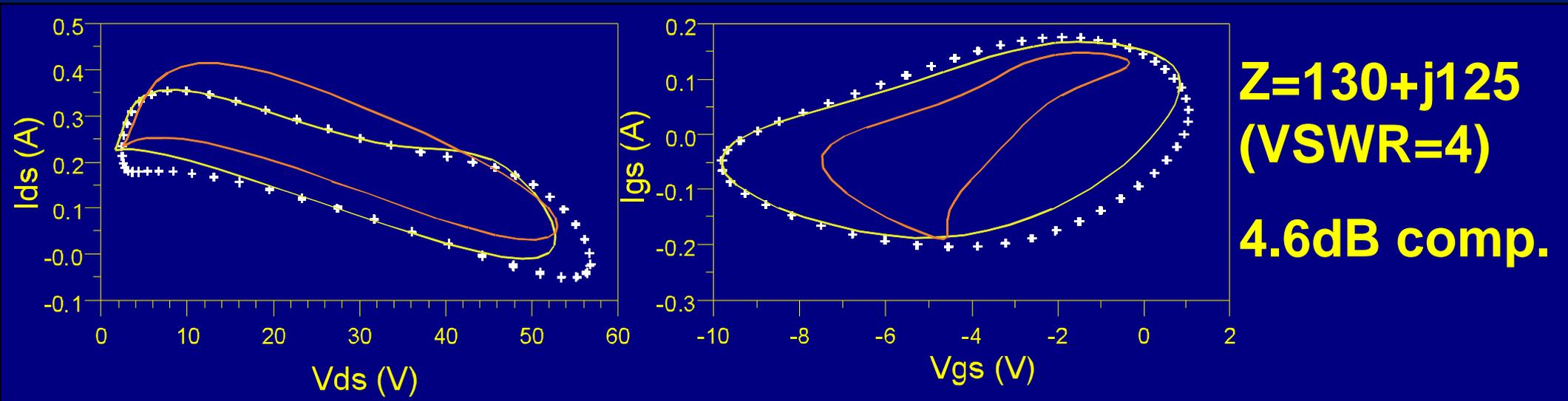
Example: Measurement on $Z=13.4+j29$ (VSWR=1.6)



- Characteristics better reproduced (especially Gamma_in and Ids)

Validation on LSNA measurements @ 5 Ghz

Time-domain measurements in class AB (25V, 200mA)



- Output current more realistic
- Strong impact on input cycles

Conclusions

- Modeling trapping effects allow reproducing better:
 - the pulsed IV curves versus the quiescent bias point.
 - the decreasing form of the output current form in large-signal
 - the large-signal measurements (larger range of Z_{load})
- Fast and easy extraction of the trapping model (1 measurement)
- Convergence of the models not affected, simulation times in H-Balance $\times 1.5$

Thank you for your
attention



